



THROX Exhaust Stack Particulate Matter and Flow RATA Test Report

Prepared for:

Dow Corning Corporation

Dow Corning Corporation
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Midland, MI 48640

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Project No. 13-4462.00
January 8, 2014

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EXECUTIVE SUMMARY

BT Environmental Consulting, Inc. (BTEC) was retained by Dow Corning Corporation (Dow) to conduct a Relative Accuracy Test Audit (RATA) and an emissions rate compliance test of the THROX unit at the Dow facility in Midland, Michigan. The emissions test program was conducted on November 19-21, 2013.

Testing of Throx exhaust consisted of eleven 21-minute test runs on the flowrate, CO₂, and NO_x monitors, triplicate 60-minute test runs for PM₁₀, CO, and VOC. Triplicate 60-minute test runs for PM₁₀ were also conducted on the Throx inlet. The emissions test program was required by MDEQ Air Quality Division Permit to Install 91-07D. The overall results of the emissions test program are detailed by Table I.

**Table I
Overall Emission Summary
Test Date: November 19-21, 2012**

| Source | Pollutant | Emission Result | Emission Limit |
|---------------|----------------------|------------------------|-----------------------|
| Throx Inlet | PM ₁₀ | 25.96 lb/hr | NA |
| Throx Exhaust | PM ₁₀ | 1.16 lb/hr | 3.5 lb/hr |
| | CO | 0.01 lb/hr | 90 ton/yr |
| | VOC | 0.03 lb/hr | 6.6 lb/hr |
| | Flow RATA | 6.8% | 20% |
| | CO ₂ RATA | 7.5% | 20% |
| | NO _x RATA | 0.5% | 20% |

TABLE OF CONTENTS

1. INTRODUCTION.....1

 1.A IDENTIFICATION, LOCATION, AND DATES OF TEST1

 1.B PURPOSE OF TESTING.....1

 1.C SOURCE DESCRIPTION1

 1.D TEST PROGRAM CONTACTS1

2. SUMMARY OF RESULTS.....2

 2.A OPERATING DATA.....2

 2.B APPLICABLE PERMIT.....2

 2.C RESULTS2

3. SOURCE DESCRIPTION.....2

 3.A PROCESS DESCRIPTION3

 3.B PROCESS FLOW DIAGRAM3

 3.C RAW AND FINISHED MATERIALS3

 3.D PROCESS CAPACITY3

 3.E PROCESS INSTRUMENTATION.....3

4. SAMPLING AND ANALYTICAL PROCEDURES3

 4.A SAMPLING TRAIN AND FIELD PROCEDURES3

 4.B RECOVERY AND ANALYTICAL PROCEDURES6

 4.C SAMPLING PORTS.....6

 4.D TRAVERSE POINTS6

5. TEST RESULTS AND DISCUSSION6

 5.A RESULTS TABULATION6

 5.B DISCUSSION OF RESULTS6

 5.C SAMPLING PROCEDURE VARIATIONS.....6

 5.D PROCESS OR CONTROL DEVICE UPSETS.....7

 5.E CONTROL DEVICE MAINTENANCE7

 5.F RE-TEST7

 5.G AUDIT SAMPLE ANALYSES7

 5.H CALIBRATION SHEETS.....7

 5.I SAMPLE CALCULATIONS.....7

 5.J FIELD DATA SHEETS7

 5.K LABORATORY DATA7

TABLE OF CONTENTS (continued)

SUMMARY TABLES

| | |
|---------|--|
| Table 1 | Test Personnel Summary |
| Table 2 | Overall Emissions Summary |
| Table 3 | THROX Inlet Particulate Matter Emission Rates |
| Table 4 | THROX Exhaust Particulate Matter Emission Rates |
| Table 5 | THROX Exhaust Flow RATA Results Summary |
| Table 6 | THROX Exhaust CO ₂ % RATA Results Summary |
| Table 7 | THROX Exhaust NO _x ppm RATA Results Summary |
| Table 8 | THROX Exhaust CO and VOC Emission Rates |

FIGURES

| | |
|----------|--|
| Figure 1 | – Throx Inlet Traverse Point Diagram |
| Figure 2 | – Throx Exhaust Traverse Point Diagram |
| Figure 3 | – USEPA Method 4 Sampling Train Drawing |
| Figure 4 | – USEPA Method 5/202 Sampling Train Drawing |
| Figure 5 | – USEPA Method 25A Sampling Train Drawing |
| Figure 6 | – USEPA Method 3A/7E/10 Sampling Train Drawing |

APPENDIX

| | |
|------------|---|
| Appendix A | AQD Test Plan/Report Format Guideline |
| Appendix B | Field and Computer Generated Raw Data and Field Notes |
| Appendix C | Dow Corning RATA and Process Data |
| Appendix D | Equipment Calibration and Span Gas Documents |
| Appendix E | Example Calculations |
| Appendix F | Laboratory Analytical Results |



1. Introduction

BT Environmental Consulting, Inc. (BTEC) was retained by Dow Corning Corporation (Dow) to conduct a Relative Accuracy Test Audit (RATA) and an emissions rate compliance test of the THROX unit at the Dow facility in Midland, Michigan. The emissions test program was conducted on November 19-21, 2013. The purpose of this report is to document the results of the test program.

AQD has published a guidance document entitled "Format for Submittal of Source Emission Test Plans and Reports" (February 2008). The following is a summary of the emissions test program and results in the format suggested by the aforementioned document.

1.a Identification, Location, and Dates of Test

Sampling and analysis for the emission test program was conducted on November 19 and 21, 2013 at the Dow Corning facility located in Midland, Michigan. Testing of Throx exhaust consisted of eleven 21-minute test runs on the flowrate, CO₂, and NO_x monitors, triplicate 60-minute test runs for PM₁₀, CO, and VOC. Triplicate 60-minute test runs for PM₁₀ were also conducted on the Throx inlet

1.b Purpose of Testing

The purpose of testing was to quantify PM₁₀, CO, and VOC emissions from the Throx Exhaust, PM₁₀ emissions from the Throx Inlet, and perform a RATA on the Throx Exhaust flow, CO₂, and NO_x monitors.

1.c Source Description

The emission unit is a thermal oxidizer followed in series by a quench, a caustic scrubber, and two ionizing wet scrubbers.

1.d Test Program Contacts

The contact for the source and test report is:

Mr. Michael Gruber, II
Environmental Manager
Dow Corning Corporation
P.O. Box 995, Mail#065
Midland, Michigan 48686
(989) 496-5539

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Names and affiliations for personnel who were present during the testing program are summarized by Table 1.

**Table 1
Test Personnel**

| Name and Title | Affiliation | Telephone |
|---|--|------------------|
| Mr. Michael Gruber, II Environmental Manager | Dow Corning Corporation P.O. Box 995, Mail#065 Midland, Michigan 48686 | (989) 496-5539 |
| Mr. Barry Boulianne Senior Project Manager | BTEC 4949 Fernlee Avenue Royal Oak, MI 48073 | (248) 548-8070 |
| Mr. Brandon Chase Staff Environmental Engineer | BTEC 4949 Fernlee Avenue Royal Oak, MI 48073 | (248) 548-8070 |
| Mr. Jeff Peitzsch Staff Environmental Engineer | BTEC 4949 Fernlee Avenue Royal Oak, MI 48073 | (248) 548-8070 |
| Mr. Kenny Felder Environmental Technician | BTEC 4949 Fernlee Avenue Royal Oak, MI 48073 | (248) 548-8070 |

2. Summary of Results

Sections 2.a through 2.d summarize the results of the emissions compliance test program.

2.a Operating Data

Process operating data collected during the emissions test program is included in Appendix C.

2.b Applicable Permit

The Dow facility is covered by Permit No. MI-ROP-A4043-2008.

The emissions test program was required by AQD Permit No. 91-07D.

2.c Results

The overall results of the emissions test program are detailed by Table 2. Detailed results for each test run are included in Tables 3-8.

3. Source Description

Sections 3.a through 3.e provide a detailed description of the process.

3.a Process Description

The emission unit is a thermal oxidizer followed in series by a quench; a caustic scrubber, and two ionizing wet scrubbers.

3.b Process Flow Diagram

Due to the simplicity of the process, a process flow diagram is not necessary.

3.c Raw and Finished Materials

The raw materials include natural gas and process operations exhaust gas.

3.d Process Capacity

The FGTHROX has a 99.9% destruction efficiency for hydrocarbons and is nominally rated for approximately 95 MMBTU/hr heat input.

3.e Process Instrumentation

Process instrumentation is summarized by the operating data provided in Appendix C.

4. Sampling and Analytical Procedures

Sections 4.a through 4.d provide a summary of the sampling and analytical procedures used.

4.a Sampling Train and Field Procedures

Sampling and analysis procedures utilized the following test methods codified at Title 40, Part 60, Appendix A of the Code of Federal Regulations:

- Method 1 - *“Sample and Velocity Traverses for Stationary Sources”*
- Method 2 - *“Determination of Stack Gas Velocity and Volumetric Flowrate”*
- Method 3A - *“Determination of Molecular Weight of Dry Stack Gas”*
- Method 4 - *“Determination of Moisture Content in Stack Gases”*
- Method 5 - *“Determination of Particulate Emissions from Stationary Sources”*
- Method 7E - *“Determination of Nitrogen Oxide Emissions from Stationary Sources”*

- Method 10 - *“Determination of Carbon Monoxide Emissions from Stationary Sources”*
- Method 25A - *“Determination of Total Gaseous Organic Concentration using a Flame Ionization Analyzer”*
- Method 202 - *“Determination of Condensable Particulate Emissions from Stationary Sources”*

Stack gas velocity traverses were conducted in accordance with the procedures outlined in Methods 1 and 2. A cyclonic flow evaluation was conducted at each sampling location. An S-type pitot tube and thermocouple assembly calibrated in accordance with Method 2, Section 4.1.1 was used to measure exhaust gas velocity pressures and temperatures during testing. Because the pitot tube dimensions outlined in Sections 2.6 through 2.8 were within the specified limits, the baseline pitot tube coefficient of 0.84 (dimensionless) was assigned for this testing.

For Method 4, BTEC's Nutech[®] Model 2010 modular isokinetic stack sampling system consisted of (1) a stainless-steel probe with glass liner, (2) a set of four Greenburg-Smith (GS) impingers with the first and third modified and the second a standard GS impinger, the first two containing 100 ml of deionized water, the third empty, and a fourth modified GS impinger containing approximately 300 g of silica gel desiccant, (3) a length of sample line, and (4) a Nutech[®] control case equipped with a pump, dry gas meter, and calibrated orifice.

40 CFR 60, Appendix A, Method 5, *“Determination of Particulate Emissions from Stationary Sources”* and 40 CFR 60, Appendix A, Method 202, *“Dry Impinger Method for Determining Condensable Particulate Emissions from Stationary Sources”* was used to measure PM concentrations and calculate PM emission rates (see Figure 4 for a schematic of the sampling train). Triplicate 60-minute test runs were conducted for each source.

BTEC's Nutech[®] Model 2010 modular isokinetic stack sampling system consisted of (1) a stainless-steel nozzle, (2) a steel probe, (3) a heated filter holder, (4) a vertical condenser, (5) an empty pot bellied impinger, (6) an empty modified Greenburg-Smith (GS) impinger, (7) unheated filter holder with a teflon filter, (8) a second modified GS impinger with 100 ml of deionized water, and a third modified GS impinger containing approximately 300 g of silica gel desiccant, (9) a length of sample line, and (10) a Nutech[®] control case equipped with a pump, dry gas meter, and calibrated orifice.

A sampling train leak test was conducted before and after each test run. After completion of the final leak test for each test run, the filter was recovered, and the nozzle and the front half of the filter holder assembly were brushed and triple rinsed with acetone. The acetone rinses were collected in a pre-cleaned sample container. The impinger train was then purged with nitrogen for one hour at a flow rate of 18 liters per minute. The CPM filter was recovered and placed in a petri dish. The back half of the filter housing, the

condenser, the pot bellied impinger, the moisture drop out impinger, and the front half of the CPM filter housing and all connecting glassware were triple rinsed with deionized water which was collected in a pre-cleaned sample container. The same glassware was then rinsed with acetone which was collected in a pre-cleaned sample container labeled as the organic fraction. The glassware was then double rinsed with hexane which was added to the same organic fraction sample bottle.

BTEC labeled each container with the test number, test location, and test date, and marked the level of liquid on the outside of the container. In addition, blank samples of the acetone, DI water, hexane, and filter were collected. BTEC personnel carried all samples to BTEC's laboratory (for filter and acetone gravimetric analysis) in Royal Oak, Michigan. DI water and organic samples were couriered by Maxxam personnel to Maxxam's lab in Mississauga, Ontario for analysis.

Exhaust NO_x content was measured using a Teledyne Model T-200H NO_x gas analyzer, and the CO and CO₂ content were measured using a Teledyne Model 300EM CO/CO₂ gas analyzer. A sample of the gas stream was drawn through an insulated stainless-steel probe with an in-line glass fiber filter to remove any particulate, a heated Teflon[®] sample line, and through an electronic sample conditioner to remove the moisture from the sample before it enters the analyzer. Data was recorded at 4-second intervals on a PC equipped with data acquisition software.

Volatile Organic compound (VOC) concentrations were measured according to 40 CFR 60, Appendix A, Method 25A. A sample of the gas stream was drawn through a stainless steel probe with an in-line glass fiber filter to remove any particulate, and a heated Teflon[®] sample line to prevent the condensation of any moisture from the sample before it enters the analyzer. Data was recorded at 4-second intervals on a PC equipped with Labview[®] II data acquisition software. BTEC used a VIG Model 20 THC hydrocarbon analyzer to determine the VOC concentration.

The VIG THC hydrocarbon analyzer channels a fraction of the gas sample through a capillary tube that directs the sample to the flame ionization detector (FID), where the hydrocarbons present in the sample are ionized into carbon. The carbon concentration is then determined by the detector in parts per million (ppm). This concentration is transmitted to the data acquisition system (DAS) at 4-second intervals in the form of an analog signal, specifically voltage, to produce data that can be averaged over the duration of the testing program. This data is then used to determine the average ppm for total hydrocarbons (THC) using the equivalent units of propane (calibration gas). The analyzer was calibrated for a range of 0 to 100 ppm.

In accordance with Method 25A, a 3-point (zero, mid, and high) calibration check was performed on the THC analyzer. Calibration drift checks were performed at the completion of each run.

4.b Recovery and Analytical Procedures

Recovery and analytical procedures were described in Section 4.a.

4.c Sampling Ports

A diagram of the stack indicating traverse point locations and stack dimensions is included as Figures 1-2.

4.d Traverse Points

A diagram of the stack indicating traverse point locations and stack dimensions is included as Figures 1-2.

5. Test Results and Discussion

Sections 5.a through 5.k provide a summary of the test results.

5.a Results Tabulation

The overall results of the emissions test program are detailed by Table 2.

Table 2
Overall Emission Summary
Test Date: November 19-21, 2012

| Source | Pollutant | Emission Result | Emission Limit |
|---------------|----------------------|-----------------|----------------|
| Throx Inlet | PM ₁₀ | 25.96 lb/hr | NA |
| Throx Exhaust | PM ₁₀ | 1.16 lb/hr | 3.5 lb/hr |
| | CO | 0.01 lb/hr | 90 ton/yr |
| | VOC | 0.03 lb/hr | 6.6 lb/hr |
| | Flow RATA | 6.8% | 20% |
| | CO ₂ RATA | 7.5% | 20% |
| | NOx RATA | 0.5% | 20% |

5.b Discussion of Results

All emission results are below the emission limits.

5.c Sampling Procedure Variations

There were no variations in the sampling procedures from that specified by the emissions test plan.

JAN 22 2014

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Dow process monitor recording went off-line during Run 3 of the RATA. Run 3 has been discarded.

5.e Control Device Maintenance

There was no non-routine control equipment maintenance performed immediately prior to the emissions test program.

5.f Re-Test

The emissions test program was not a re-test.

5.g Audit Sample Analyses

No audit samples were collected as part of the test program.

5.h Calibration Sheets

Relevant equipment calibration documents are provided in Appendix C.

5.i Sample Calculations

Sample calculations are provided in Appendix D.

5.j Field Data Sheets

Field documents relevant to the emissions test program are presented in Appendix B.

5.k Laboratory Data

Laboratory analytical results are available in Appendix F.

**Table 4
Throx Exhaust Particulate Matter Emission Rates**

| Company Source Designation Test Date | Dow Throx | | | Average |
|--|--------------|------------|------------|----------|
| | 11/21/2013 | 11/21/2013 | 11/21/2013 | |
| Meter/Nozzle Information | | | | |
| Meter Temperature Tm (F) | 57.7 | 65.0 | 67.3 | 63.3 |
| Meter Pressure - Pm (in. Hg) | 29.7 | 29.6 | 29.6 | 29.6 |
| Measured Sample Volume (Vm) | 53.7 | 37.2 | 36.9 | 42.6 |
| Sample Volume (Vm-Std ft3) | 54.4 | 37.1 | 36.6 | 42.7 |
| Sample Volume (Vm-Std m3) | 1.54 | 1.05 | 1.04 | 1.21 |
| Condensate Volume (Vw-std) | 11.189 | 7.497 | 7.502 | 8.729 |
| Gas Density (Ps(std) lbs/ft3) (wet) | 0.0697 | 0.0698 | 0.0698 | 0.0698 |
| Gas Density (Ps(std) lbs/ft3) (dry) | 0.0745 | 0.0745 | 0.0745 | 0.0745 |
| Total weight of sampled gas (m g lbs) (wet) | 4.58 | 3.11 | 3.08 | 3.59 |
| Total weight of sampled gas (m g lbs) (dry) | 4.06 | 2.76 | 2.73 | 3.18 |
| Nozzle Size - An (sq. ft.) | 0.001294 | 0.000860 | 0.000860 | 0.001004 |
| Isokinetic Variation - I | 95.3 | 95.9 | 95.8 | 95.7 |
| Stack Data | | | | |
| Average Stack Temperature - Ts (F) | 135.9 | 135.2 | 135.3 | 135.4 |
| Molecular Weight Stack Gas- dry (Md) | 28.8 | 28.8 | 28.8 | 28.8 |
| Molecular Weight Stack Gas-wet (Ms) | 27.0 | 27.0 | 27.0 | 27.0 |
| Stack Gas Specific Gravity (Gs) | 0.932 | 0.933 | 0.932 | 0.932 |
| Percent Moisture (Bws) | 17.05 | 16.82 | 17.01 | 16.96 |
| Water Vapor Volume (fraction) | 0.1705 | 0.1682 | 0.1701 | 0.1696 |
| Pressure - Ps ("Hg) | 29.5 | 29.5 | 29.5 | 29.5 |
| Average Stack Velocity - Vs (ft/sec) | 16.9 | 17.2 | 17.0 | 17.0 |
| Area of Stack (ft2) | 15.9 | 15.9 | 15.9 | 15.9 |
| Exhaust Gas Flowrate | | | | |
| Flowrate ft ³ (Actual) | 16,124 | 16,371 | 16,204 | 16,233 |
| Flowrate ft ³ (Standard Wet) | 14,096 | 14,330 | 14,182 | 14,202 |
| Flowrate ft ³ (Standard Dry) | 11,692 | 11,920 | 11,769 | 11,794 |
| Flowrate m ³ (standard dry) | 331 | 338 | 333 | 334 |
| Total Particulate Weights (mg) | | | | |
| Total Nozzle/Probe/Filter | 34.5 | 23.7 | 26.6 | 28.3 |
| Organic Condensable Particulate | 1.3 | 1.1 | 0.0 | 0.8 |
| Inorganic Condensable Particulate | 3.0 | 5.3 | 3.9 | 4.1 |
| Condensable Blank Correction | 2.0 | 2.0 | 2.0 | 2.0 |
| Total Condensable Particulate | 2.3 | 4.4 | 1.9 | 2.9 |
| Total Filterable and Condensable Particulate | 36.8 | 28.1 | 28.5 | 31.1 |
| Filterable Particulate Concentration | | | | |
| lb/1000 lb (wet) | 0.017 | 0.017 | 0.019 | 0.017 |
| lb/1000 lb (dry) | 0.019 | 0.019 | 0.022 | 0.020 |
| mg/dscm (dry) | 22.4 | 22.6 | 25.7 | 23.5 |
| gr/dscf | 0.010 | 0.010 | 0.011 | 0.010 |
| Filterable Particulate Emission Rate | | | | |
| lb/ hr | 0.98 | 1.01 | 1.14 | 1.04 |
| Condensable Particulate Concentration | | | | |
| lb/1000 lb (wet) | 0.001 | 0.003 | 0.001 | 0.002 |
| lb/1000 lb (dry) | 0.001 | 0.004 | 0.002 | 0.002 |
| mg/dscm (dry) | 1.5 | 4.2 | 1.8 | 2.5 |
| gr/dscf | 0.001 | 0.002 | 0.001 | 0.001 |
| Condensable Particulate Emission Rate | | | | |
| lb/ hr | 0.07 | 0.19 | 0.08 | 0.11 |
| Total Particulate Concentration | | | | |
| lb/1000 lb (wet) | 0.018 | 0.020 | 0.020 | 0.019 |
| lb/1000 lb (dry) | 0.020 | 0.022 | 0.023 | 0.022 |
| mg/dscm (dry) | 23.9 | 26.8 | 27.5 | 26.0 |
| gr/dscf | 0.010 | 0.012 | 0.012 | 0.011 |
| Total Particulate Emission Rate | | | | |
| lb/ hr | 1.05 | 1.20 | 1.22 | 1.16 |

TABLE 5

Throx Exhaust Flow RATA Results Summary

Dow Corning Corp.

Midland, Michigan

THROX

| FLOW Relative Accuracy | | | | | |
|-------------------------------|--------------------------|--------------------|---------------------|---------|---------|
| Relative Accuracy: | | 6.8 | | | |
| Run # | Time* | RM <u>KSCFM</u> | CEM <u>KSCFM</u> | Diff | %Diff |
| 1 | 7:32-7:53 | 17.1 | 18.9 | -1.7932 | -0.10 |
| 2 | 8:06-8:27 | 18.8 | 21.1 | -2.2991 | -0.12 |
| 4 | 11:20-11:41 | 19.5 | 21.1 | -1.5778 | -0.08 |
| 5 | 11:56-12:17 | 20.0 | 20.8 | -0.8358 | -0.04 |
| 6 | 12:30-12:51 | 20.5 | 21.7 | -1.2487 | -0.06 |
| 7 | 13:01-13:22 | 21.2 | 21.7 | -0.5380 | -0.03 |
| 8 | 13:34-13:55 | 19.2 | 20.1 | -0.8999 | -0.05 |
| 9 | 14:06-14:27 | 18.4 | 19.0 | -0.6313 | -0.03 |
| 10 | 14:40-15:01 | 20.1 | 20.0 | 0.0524 | 0.00 |
| 11 | 15:12-15:33 | 19.8 | 19.8 | -0.0446 | 0.00 |
| 12 | | | | #VALUE! | #VALUE! |
| 13 | | | | #VALUE! | #VALUE! |
| | | 19.5 | 20.3 | -0.835 | -0.044 |
| | Sdev | | 0.6312 | | |
| | CC | | 0.4852 | | |
| | RA (based on Ref. Meth.) | | 6.8% | | |

*: Time stamp is according to Dow's clock. BTEC time is 10 minutes behind Dow.

i.e., 7:42 BTEC time = 7:32 Dow time

Note: Run 3 is omitted because Dow process monitoring recording went offline.

Confidence Coefficient =

$$n=9$$

$$t = 2.306$$

$$CC = \frac{t}{0.975} \frac{S_d}{\sqrt{n}}$$

P.S. 2 Equation 2-5

Standard Deviation =

$$S_d = \left[\frac{\sum_{i=1}^n d_i^2 - \frac{(\sum_{i=1}^n d_i)^2}{n}}{n-1} \right]^{1/2}$$

P.S. 2 Equation 2-4

Relative Accuracy =

RM=Reference Monitor

$$RA = \frac{|d| + |cc|}{RM} \times 100$$

P.S. 2 Equation 2-6

RA calculated as specified in Performance Specification 2, Appendix B, 40 CFR 60 - Equation 2-4

As specified in P.S. 2, subsection 8.4.4, three sets of test runs may be rejected, these rejected test runs are high-lighted in the table

TABLE 6

Throx Exhaust CO₂ % RATA Results Summary

Dow Corning Corp.

Midland, Michigan

THROX

| CO ₂ % Relative Accuracy | | | | | |
|-------------------------------------|-------------|--------------------------|----------|---------|---------|
| Relative Accuracy: | | | | 7.5 | |
| Run # | Time* | RM % | CEM % | Diff | %Diff |
| 1 | 7:32-7:53 | 1.89 | 1.7 | 0.1900 | 0.10 |
| 2 | 8:06-8:27 | 1.94 | 1.8 | 0.1400 | 0.07 |
| 4 | 11:20-11:41 | 2.69 | 2.5 | 0.1900 | 0.07 |
| 5 | 11:56-12:17 | 2.37 | 2.2 | 0.1700 | 0.07 |
| 6 | 12:30-12:51 | 2.39 | 2.2 | 0.1900 | 0.08 |
| 7 | 13:01-13:22 | 2.38 | 2.2 | 0.1800 | 0.08 |
| 8 | 13:34-13:55 | 2.46 | 2.3 | 0.1600 | 0.07 |
| 9 | 14:06-14:27 | 2.49 | 2.4 | 0.0900 | 0.04 |
| 10 | 14:40-15:01 | 2.37 | 2.3 | 0.0700 | 0.03 |
| 11 | 15:12-15:33 | 2.41 | 2.3 | 0.1100 | 0.05 |
| 12 | | | | #VALUE! | #VALUE! |
| 13 | | | | #VALUE! | #VALUE! |
| | | 2.389 | 2.24 | 0.144 | 0.061 |
| | | Sdev | 0.0448 | | |
| | | CC | 0.0344 | | |
| | | RA (based on Ref. Meth.) | 7.5% | | |

*: Time stamp is according to Dow's clock. BTEC time is 10 minutes behind Dow.
i.e., 7:42 BTEC time = 7:32 Dow time

Note: Run 3 is omitted because Dow process monitoring recording went offline.

Confidence Coefficient =

$$n=9$$

$$t=2.306$$

$$CC = t_{0.975} \frac{S_d}{\sqrt{n}}$$

P.S. 2 Equation 2-5

Standard Deviation =

$$S_d = \left[\frac{\sum_{i=1}^n d_i^2 - \frac{(\sum_{i=1}^n d_i)^2}{n}}{n-1} \right]^{1/2}$$

P.S. 2 Equation 2-4

Relative Accuracy =

RM=Reference Monitor

$$RA = \frac{|\bar{d}| + |cc|}{RM} \times 100$$

P.S. 2 Equation 2-6

RA calculated as specified in Performance Specification 2, Appendix B, 40 CFR 60 -
Equation 2-4

As specified in P.S. 2, subsection 8.4.4, three sets of test runs may be rejected,
these rejected test runs are high-lighted in the table

TABLE 7

Throx Exhaust NOx ppm RATA Results Summary
 Dow Corning Corp.
 Midland, Michigan
 THROX

| NO _x PPM Relative Accuracy | | | | | |
|---------------------------------------|-------------|--------------------------|--------------|---------|---------|
| Relative Accuracy: | | 0.5 | | | |
| Run # | Time* | RM PPMVD | CEM PPMVD | Diff | %Diff |
| 1 | 7:32-7:53 | 64.14 | 63.0 | 1.1400 | 0.02 |
| 2 | 8:06-8:27 | 58.43 | 58.5 | -0.0700 | 0.00 |
| 4 | 11:20-11:41 | 47.79 | 48.1 | -0.3100 | -0.01 |
| 5 | 11:56-12:17 | 57.84 | 57.8 | 0.0400 | 0.00 |
| 6 | 12:30-12:51 | 51.38 | 51.1 | 0.2800 | 0.01 |
| 7 | 13:01-13:22 | 49.55 | 49.1 | 0.4500 | 0.01 |
| 8 | 13:34-13:55 | 50.53 | 50.6 | -0.0700 | 0.00 |
| 9 | 14:06-14:27 | 52.56 | 52.1 | 0.4600 | 0.01 |
| 10 | 14:40-15:01 | 53.52 | 53.5 | 0.0200 | 0.00 |
| 11 | 15:12-15:33 | 56.11 | 56.3 | -0.1900 | 0.00 |
| 12 | | | | #VALUE! | #VALUE! |
| 13 | | | | #VALUE! | #VALUE! |
| | | 53.079 | 53.01 | 0.068 | 0.001 |
| | | Sdev | 0.2728 | | |
| | | CC | 0.2097 | | |
| | | RA (based on Ref. Meth.) | 0.5% | | |

*: Time stamp is according to Dow's clock. BTEC time is 10 minutes behind Dow.
 i.e., 7:42 BTEC time = 7:32 Dow time
 Note: Run 3 is omitted because Dow process monitoring recording went offline.

Confidence Coefficient = $CC = t_{\alpha/2, n-1} \frac{S_d}{\sqrt{n}}$ P.S. 2 Equation 2-5
 n=9
 t=2.306

Standard Deviation = $S_d = \left[\frac{\sum_{i=1}^n d_i^2 - \frac{(\sum_{i=1}^n d_i)^2}{n}}{n-1} \right]^{1/2}$ P.S. 2 Equation 2-4

Relative Accuracy = $RA = \frac{|d| + |cc|}{RM} \times 100$ P.S. 2 Equation 2-6
 RM=Reference Monitor

RA calculated as specified in Performance Specification 2, Appendix B, 40 CFR 60 - Equation 2-4

As specified in P.S. 2, subsection 8.4.4, three sets of test runs may be rejected, these rejected test runs are high-lighted in the table

Table 8
Throx Exhaust CO and VOC Emission Rates
Dow Corning
Midland, Michigan
BTEC Project No. 13-4462
Sampling Dates: November 21, 2013

| Parameter | Run 1 | Run 2 | Run 3 | Average |
|--|-------------|-------------|-------------|-------------|
| Test Run Date | 11/21/2013 | 11/21/2013 | 11/21/2013 | |
| Test Run Time | 11:06-12:06 | 12:35-13:35 | 14:14-15:14 | |
| Outlet Flowrate (dscfm) | 11,692 | 11,920 | 11,769 | 11,794 |
| Outlet Flowrate (scfm) | 14,096 | 14,330 | 14,182 | 14,202 |
| Outlet Carbon Monoxide Concentration (ppmv) | 0.57 | 0.66 | 0.99 | 0.74 |
| Outlet CO Concentration (ppmv, corrected as per USEPA 7E) | 0.10 | 0.35 | 0.39 | 0.28 |
| CO Emission Rate (lb/hr) | 0.03 | 0.03 | 0.05 | 0.04 |
| CO Emission Rate (lb/hr) (corrected as per USEPA 7E) | 0.01 | 0.02 | 0.02 | 0.01 |
| Outlet VOC Concentration (ppmv as propane) | 1.20 | 0.21 | 0.24 | 0.55 |
| Outlet VOC Concentration (ppmv, corrected as per USEPA 7E) | 0.81 | 0.00 | 0.14 | 0.32 |
| VOC Emission Rate as Propane (lb/hr) | 0.12 | 0.02 | 0.02 | 0.05 |
| VOC Emission Rate as Propane(lb/hr) (corrected as per USEPA 7E) | 0.08 | 0.00 | 0.01 | 0.03 |

scfm = standard cubic feet per minute

dscfm = dry standard cubic feet per minute

ppmv = parts per million on a volume-to-volume basis

lb/hr = pounds per hour

MW = molecular weight (CO = 28.01, C₃H₈ = 44.10)

24.14 = molar volume of air at standard conditions (70°F, 29.92" Hg)

35.31 = ft³ per m³

453600 = mg per lb

Equations

lb/hr = ppmv * MW/24.14 * 1/35.31 * 1/453,600 * *scfm* * 60 for VOC

lb/hr = ppmv * MW/24.14 * 1/35.31 * 1/453,600 * *dscfm* * 60

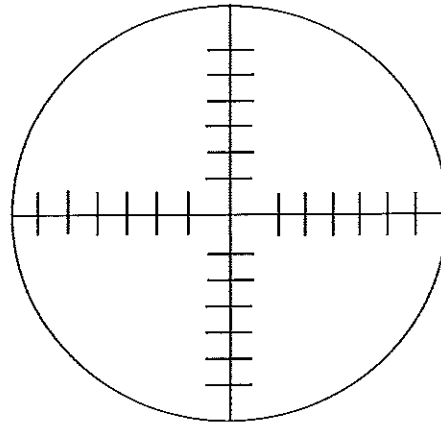
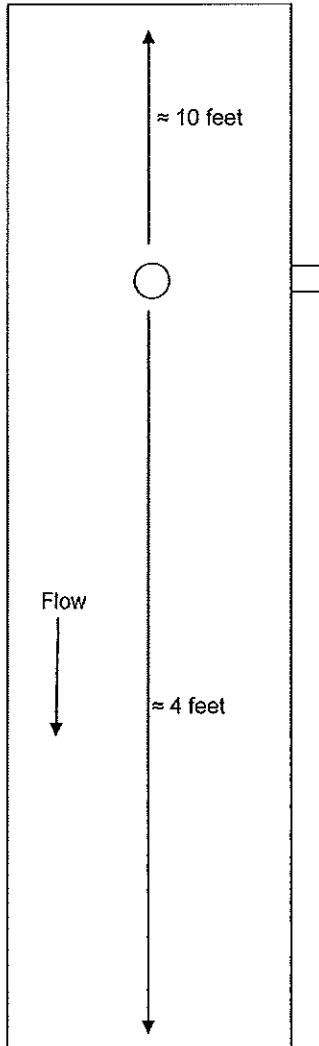
Table 3
Throx Inlet Particulate Matter Emission Rates

| Company Source Designation Test Date | Dow Throx Inlet | | | Average |
|--|--------------------|------------|------------|----------|
| | 11/21/2013 | 11/21/2013 | 11/21/2013 | |
| Meter/Nozzle Information | | | | |
| | P-1 | P-2 | P-3 | Average |
| Meter Temperature Tm (F) | 56.6 | 62.0 | 63.3 | 60.6 |
| Meter Pressure - Pm (in. Hg) | 29.7 | 29.6 | 29.6 | 29.6 |
| Measured Sample Volume (Vm) | 32.8 | 18.3 | 17.3 | 22.8 |
| Sample Volume (Vm-Std ft3) | 33.6 | 18.5 | 17.4 | 23.2 |
| Sample Volume (Vm-Std m3) | 0.95 | 0.52 | 0.49 | 0.66 |
| Condensate Volume (Vw-std) | 8.624 | 4.889 | 4.291 | 5.935 |
| Gas Density (Ps(std) lbs/ft3) (wet) | 0.0688 | 0.0687 | 0.0690 | 0.0689 |
| Gas Density (Ps(std) lbs/ft3) (dry) | 0.0746 | 0.0746 | 0.0746 | 0.0746 |
| Total weight of sampled gas (m g lbs) (wet) | 2.91 | 1.61 | 1.50 | 2.00 |
| Total weight of sampled gas (m g lbs) (dry) | 2.51 | 1.38 | 1.30 | 1.73 |
| Nozzle Size - An (sq. ft.) | 0.000759 | 0.000346 | 0.000346 | 0.000484 |
| Isokinetic Variation - I | 94.6 | 101.7 | 101.8 | 99.4 |
| Stack Data | | | | |
| Average Stack Temperature - Ts (F) | 146.8 | 145.3 | 145.3 | 145.8 |
| Molecular Weight Stack Gas- dry (Md) | 28.8 | 28.8 | 28.8 | 28.8 |
| Molecular Weight Stack Gas-wet (Ms) | 26.6 | 26.6 | 26.7 | 26.6 |
| Stack Gas Specific Gravity (Gs) | 0.920 | 0.918 | 0.922 | 0.920 |
| Percent Moisture (Bws) | 20.42 | 20.92 | 19.76 | 20.36 |
| Water Vapor Volume (fraction) | 0.2042 | 0.2092 | 0.1976 | 0.2036 |
| Pressure - Ps ("Hg) | 29.2 | 29.2 | 29.2 | 29.2 |
| Average Stack Velocity - Vs (ft/sec) | 19.3 | 21.7 | 20.1 | 20.3 |
| Area of Stack (ft2) | 12.6 | 12.6 | 12.6 | 12.6 |
| Exhaust Gas Flowrate | | | | |
| Flowrate ft ³ (Actual) | 14,515 | 16,325 | 15,158 | 15,333 |
| Flowrate ft ³ (Standard Wet) | 12,318 | 13,887 | 12,894 | 13,033 |
| Flowrate ft ³ (Standard Dry) | 9,803 | 10,982 | 10,346 | 10,377 |
| Flowrate m ³ (standard dry) | 278 | 311 | 293 | 294 |
| Total Particulate Weights (mg) | | | | |
| Total Nozzle/Probe/Filter | 605.6 | 319.6 | 357.4 | 427.5 |
| Organic Condensable Particulate | 2.7 | 1.4 | 2.2 | 2.1 |
| Inorganic Condensable Particulate | 6.0 | 5.7 | 4.5 | 5.4 |
| Condensable Blank Correction | 2.0 | 2.0 | 2.0 | 2.0 |
| Total Condensable Particulate | 6.7 | 5.1 | 4.7 | 5.5 |
| Total Filterable and Condensable Particulate | 612.3 | 324.7 | 362.1 | 433.0 |
| Filterable Particulate Concentration | | | | |
| lb/1000 lb (wet) | 0.459 | 0.439 | 0.526 | 0.475 |
| lb/1000 lb (dry) | 0.533 | 0.511 | 0.606 | 0.550 |
| mg/dscm (dry) | 636.2 | 610.6 | 724.4 | 657.0 |
| gr/dscf | 0.278 | 0.267 | 0.317 | 0.287 |
| Filterable Particulate Emission Rate | | | | |
| lb/ hr | 23.45 | 25.21 | 28.18 | 25.61 |
| Condensable Particulate Concentration | | | | |
| lb/1000 lb (wet) | 0.005 | 0.007 | 0.007 | 0.006 |
| lb/1000 lb (dry) | 0.006 | 0.008 | 0.008 | 0.007 |
| mg/dscm (dry) | 7.0 | 9.7 | 9.5 | 8.8 |
| gr/dscf | 0.003 | 0.004 | 0.004 | 0.004 |
| Condensable Particulate Emission Rate | | | | |
| lb/ hr | 0.26 | 0.40 | 0.37 | 0.34 |
| Total Particulate Concentration | | | | |
| lb/1000 lb (wet) | 0.464 | 0.446 | 0.533 | 0.481 |
| lb/1000 lb (dry) | 0.539 | 0.519 | 0.614 | 0.557 |
| mg/dscm (dry) | 643.2 | 620.3 | 733.9 | 665.8 |
| gr/dscf | 0.281 | 0.271 | 0.321 | 0.291 |
| Total Particulate Emission Rate | | | | |
| lb/ hr | 23.71 | 25.61 | 28.55 | 25.96 |

Figures



diameter = 48 inches



Not to Scale

| Points | Distance " |
|--------|------------|
| 1 | 1.0 |
| 2 | 3.2 |
| 3 | 5.7 |
| 4 | 8.5 |
| 5 | 12.0 |
| 6 | 17.1 |
| 7 | 30.9 |
| 8 | 36.0 |
| 9 | 39.5 |
| 10 | 42.3 |
| 11 | 44.8 |
| 12 | 47.0 |

Figure No. 1

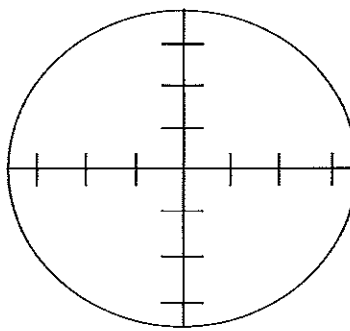
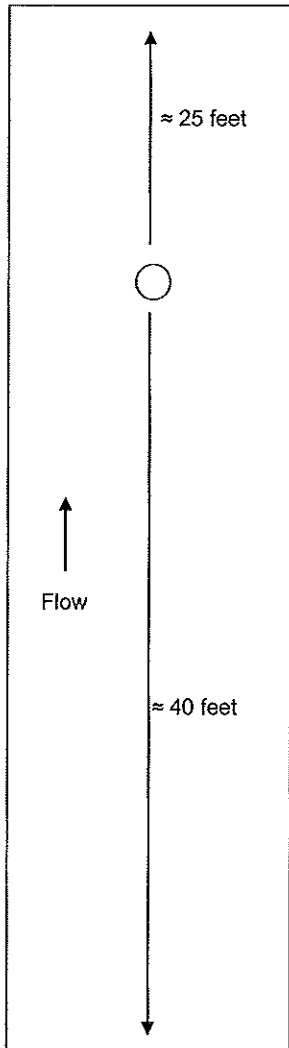
Site:
THROX Inlet
Dow Corning
Midland, Michigan

Sampling Date:
November 19-21, 2013

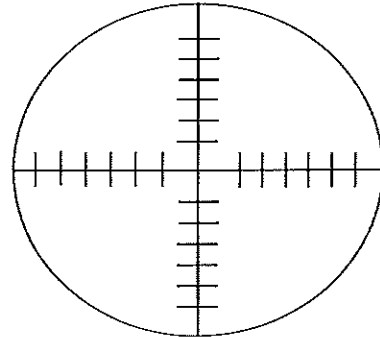
BT Environmental Consulting, Inc.
4949 Fernlee Avenue
Royal Oak, Michigan 48073



diameter = 54 inches



Traverse points used for flow measurements



Traverse points used for PM measurements

Not to Scale

| Points | Distance " | Points | Distance " |
|--------|------------|--------|------------|
| 1 | 2.4 | 1 | 1.1 |
| 2 | 7.9 | 2 | 3.6 |
| 3 | 16.0 | 3 | 6.4 |
| 4 | 38.0 | 4 | 9.6 |
| 5 | 46.1 | 5 | 13.5 |
| 6 | 51.6 | 6 | 19.2 |
| | | 7 | 34.8 |
| | | 8 | 40.5 |
| | | 9 | 44.4 |
| | | 10 | 47.6 |
| | | 11 | 50.4 |
| | | 12 | 52.9 |

Figure No. 2

Site:
THROX Exhaust
Dow Corning
Midland, Michigan

Sampling Date:
November 19-21, 2013

BT Environmental Consulting, Inc.
4949 Fernlee Avenue
Royal Oak, Michigan 48073

BTEC Inc.

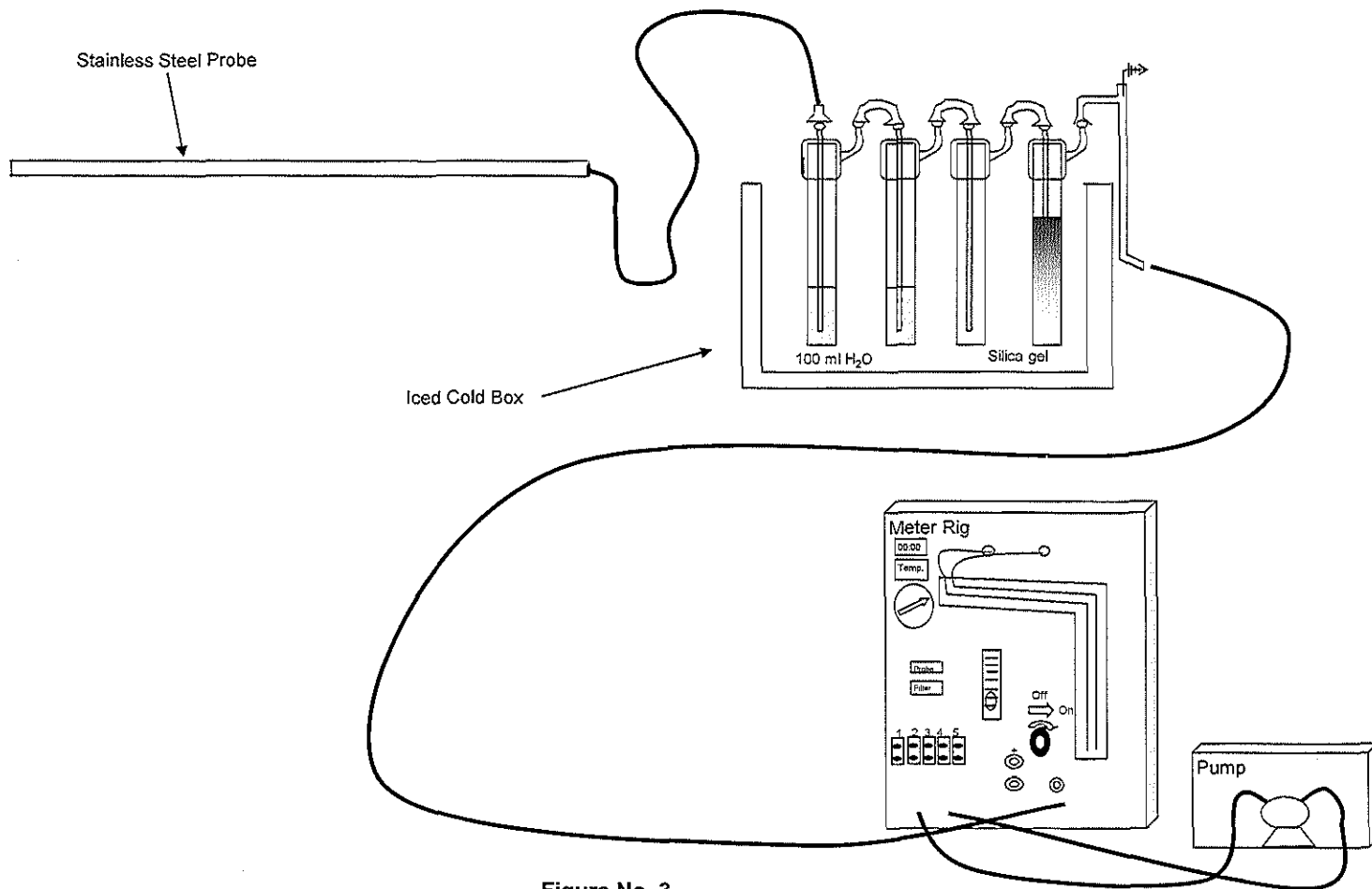


Figure No. 3

Site:
USEPA Method 4
Dow Corning
Midland, Michigan

Sampling Date:
November 19, 2013

BT Environmental Consulting, Inc.
4949 Fernlee Avenue
Royal Oak, Michigan 48073

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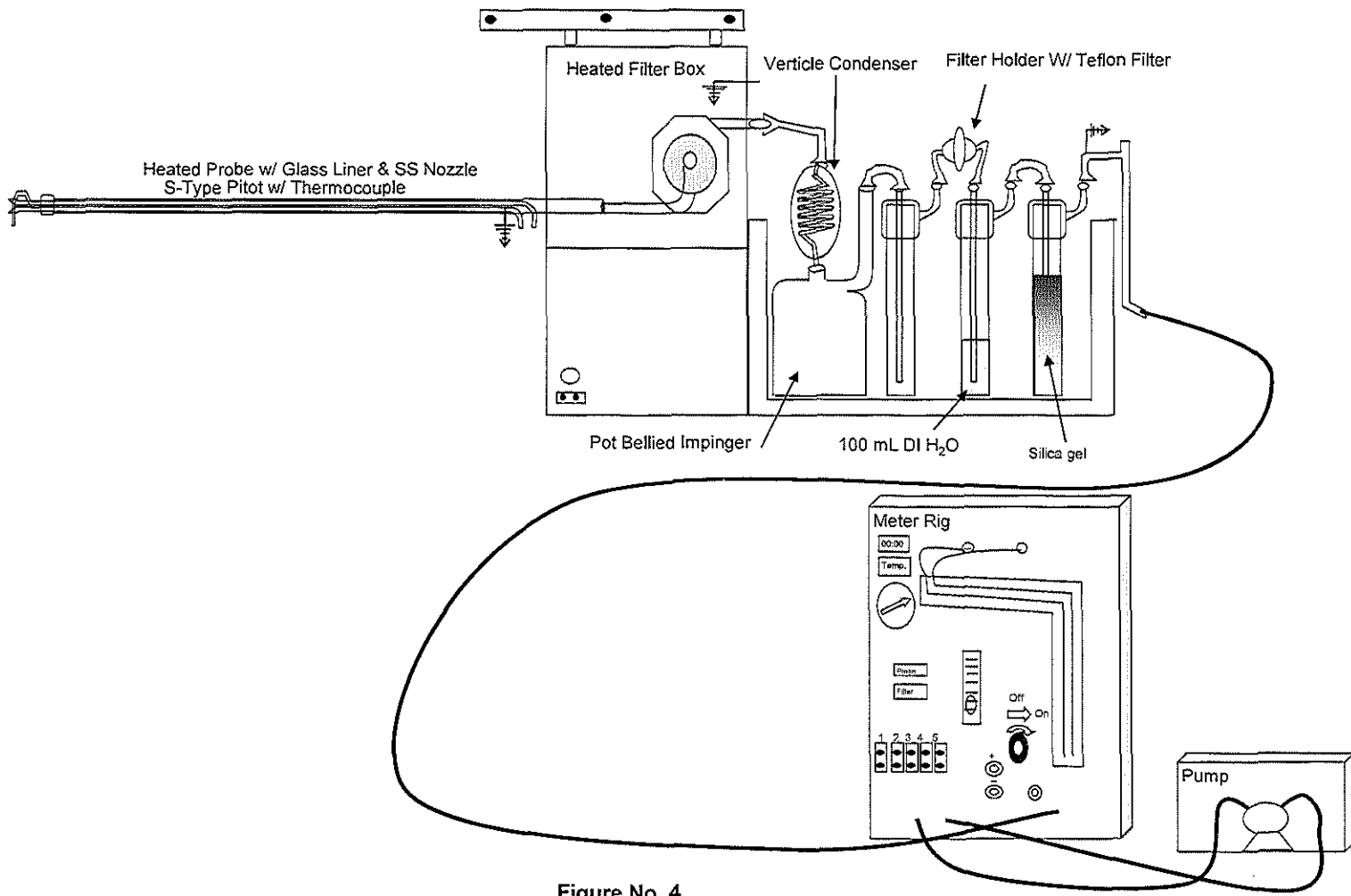


Figure No. 4

Site:
USEPA Method 5/202
Dow Corning
Midland, Michigan

Sampling Date:
November 21, 2013

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Royal Oak, Michigan 48073

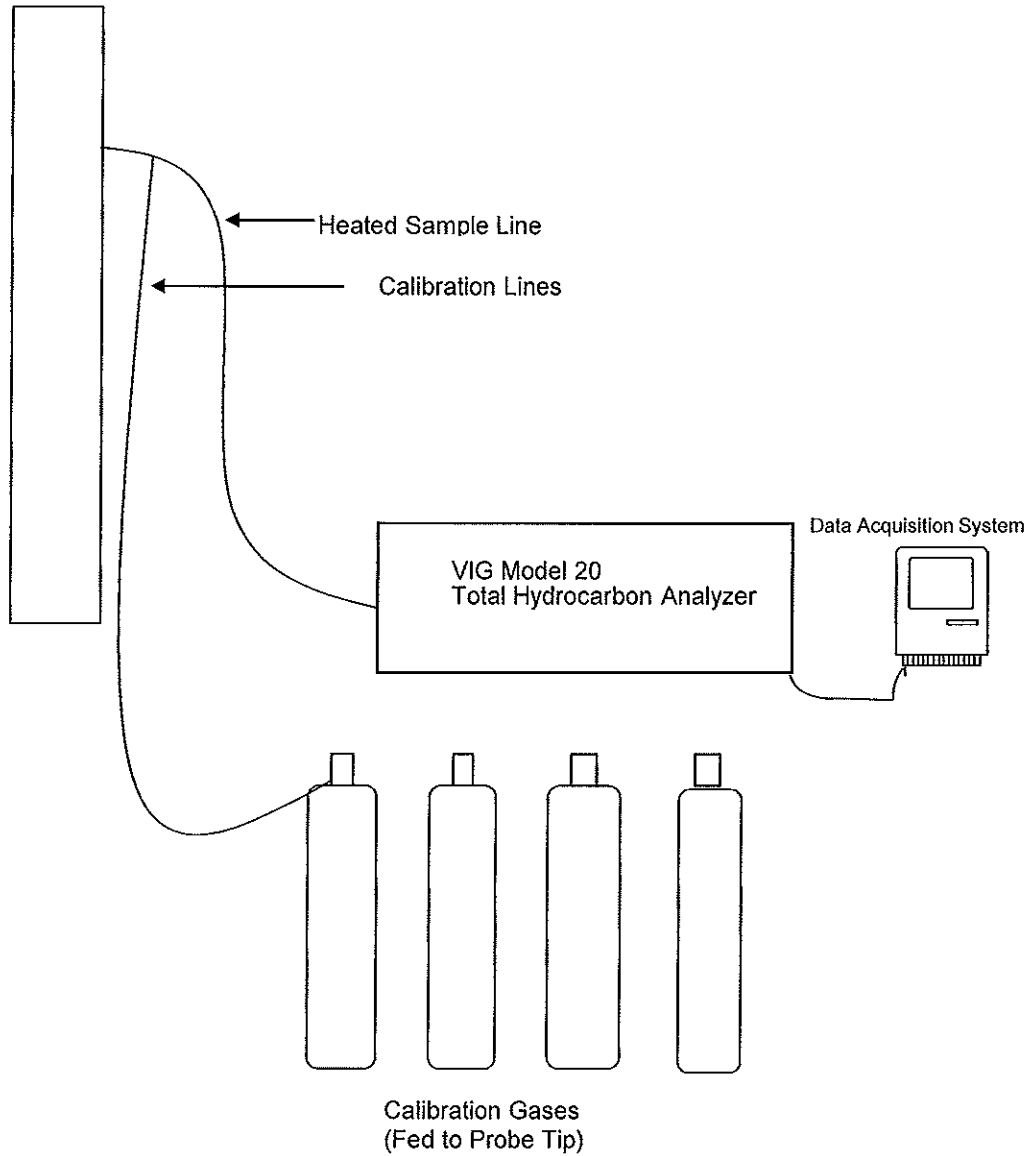


Figure No. 5

Site:
USEPA Method 25A
Dow Corning
Midland, Michigan

Sampling Date:
November 21, 2013

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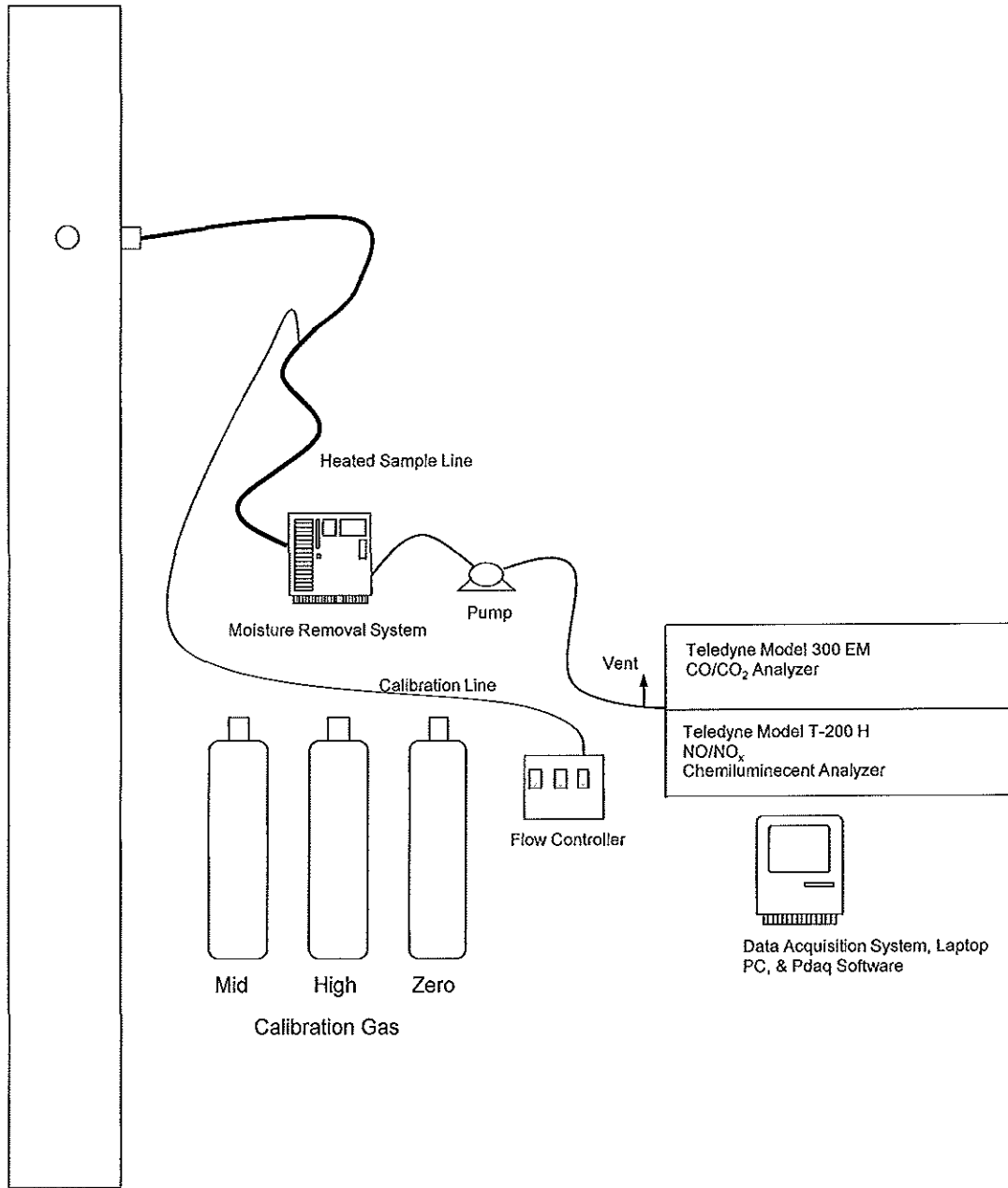


Figure No. 6

Site:
USEPA Method 3A,7E, and 10
Dow Corning
Midland, Michigan

Sampling Date:
November 19-21, 2013

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