

# **COMPLIANCE TEST REPORT**

for

**PM, PM<sub>10</sub>, VISIBLE EMISSIONS, SULFURIC ACID  
MIST, HYDROGEN CHLORIDE, HYDROGEN FLUORIDE,  
ARSENIC, LEAD, MERCURY, AND VOLATILE ORGANIC  
COMPOUNDS**

**UNIT 2 – FGD Stack**

**Monroe Power Plant  
Monroe, Michigan**

**June 17-19, 2019**

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**EXECUTIVE SUMMARY**

DTE Energy's Environmental Management and Resources, Field Services Group (EMR) performed emissions testing on the Unit 2 FGD exhaust stack located at the Monroe Power Plant, in Monroe, Michigan. The testing was required by the Michigan Department of Environment, Great Lakes, & Energy (EGLE) Permit to Install #27-13C to document stack emissions from Unit 2 FGD during normal operating conditions. Testing was conducted during the period of June 17-19, 2019.

A summary of the emission test results is shown below:

**Emissions Testing Summary  
Unit 2 FGD Stack  
Monroe Power Plant  
June 17-19, 2019**

	PM <sup>(1)</sup> (lb/MMBtu)	PM <sub>10</sub> <sup>(2)</sup> (lb/MMBtu)	Opacity (%)	VOC <sup>(3)</sup> (lb/hr)	VOC <sup>(3)</sup> (lb/MMBtu)
<b>Average</b>	<b>0.010</b>	<b>0.013</b>	<b>0</b>	<b>&lt;1.4</b>	<b>&lt;0.0002</b>
<i>Permit Limit</i>	<i>0.011</i>	<i>0.024</i>	<i>10</i>	<i>25.9</i>	<i>0.0034</i>

- (1) = Total Filterable PM
- (2) = Measured as Total Filterable PM plus Condensable PM (Per Method 202)
- (3) = As Propane

	Sulfuric Acid Mist (lb/MMBtu)	Hydrogen Chloride (lb/MMBtu)	Hydrogen Fluoride (lb/MMBtu)
<b>Average</b>	<b>&lt;0.001</b>	<b>0.0004</b>	<b>&lt;0.00010</b>
<i>Permit Limit</i>	<i>0.005</i>	<i>0.0024</i>	<i>0.00023</i>

	Arsenic (lb/MMBtu)	Lead (lb/hr)	Lead (lb/MMBtu)	Mercury (lb/yr)
<b>Average</b>	<b>0.0000007</b>	<b>0.004</b>	<b>0.0000006</b>	<b>24.7</b>
<i>Permit Limit</i>	<i>0.0000063</i>	<i>0.13</i>	<i>0.0000169</i>	<i>143.1</i>



## 1.0 INTRODUCTION

DTE Energy's Environmental Management and Resources, Field Services Group (EMR) performed emissions testing on the Unit 2 FGD exhaust stack located at the Monroe Power Plant, in Monroe, Michigan. The testing was required by the Michigan Department of Environment, Great Lakes, & Energy (EGLE) Permit to Install #27-13C to document stack emissions from Unit 2 FGD during normal operating conditions. The testing was conducted during the period of June 17-19, 2019.

Testing was performed pursuant to Title 40, *Code of Federal Regulations*, Part 60, Appendix A (40 CFR §60 App. A), Methods 1-5B, 202, 8A, 9, 25A, 26A, 29 and 30B.

The fieldwork was performed in accordance with EPA Reference Methods and EMR's Intent to Test<sup>1</sup>, which was approved in a letter by Mr. Mark Dziadosz from the Michigan Department of Environment, Great Lakes, & Energy (EGLE), dated April 18, 2019<sup>2</sup>. The following EMR personnel participated in the testing program: Mr. Mark Grigereit, Principal Engineer, Mr. Mark Thom Snyder and Mr. Jason Logan, Environmental Specialists, Mr. Fred Meinecke and Mr. Frank Kurta, Senior Engineering Technicians. Mr. Grigereit was the project Leader. Ms. Kailyn Gerzich, Environmental Engineer at Monroe Power Plant, provided process coordination for the testing program. Portions of the testing were observed by Mr. Dziadosz with the EGLE.

## 2.0 SOURCE DESCRIPTION

The Monroe Power Plant is located at 3500 E. Front Street in Monroe, Michigan. The plant has four (4) coal-fired electric generating units, referred to as Units 1, 2, 3, and 4. These units were placed in service between 1971 and 1974, and have a total electric generating capacity of 3,135 megawatts (gross). The boiler (Babcock & Wilcox) for each unit is a similar supercritical pressure, pulverized coal-fired cell burner boiler. Each boiler exhausts into a dedicated exhaust stack.

Units 1 and 4 have General Electric turbine generators, each with a rated capability of 817 gross megawatts (GMW). Units 2 and 3 have Westinghouse turbine generators, each with a rated capability of 823 GMW.

Each boiler is equipped with Research Cottrell electrostatic precipitator (ESPs), each with a rated particulate removal efficiency of 99.6%. There is a sulfur trioxide flue gas conditioning

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<sup>1</sup> EGLE, Test Plan, Submitted March 8, 2019. (Attached-Appendix A)

<sup>2</sup> EGLE, Approval Letter. (Attached-Appendix A)

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system on each unit that is only used on an “as needed basis” to lower the resistivity of the fly ash for better collection by the ESPs. None of the units are equipped with sulfuric acid mist control equipment.

Units 1 through 4 have Selective Catalytic Reduction (SCR) systems, operated to control at least 90% of the NOx emissions. The SCR's are located upstream of the respective ESP's. Each unit has wet Flue Gas Desulfurization (FGD) Scrubbers to control sulfur dioxide (SO<sub>2</sub>), other acid gases, and particulate matter emissions.

The coal blend for Unit 2 was 15% high-sulfur eastern (HSE) / 75% low-sulfur western (LSW)/ 10% Petcoke. Testing was performed while the boiler was operated at normal full load conditions (>700 GMW, approx.).

The boilers at Monroe Power Plant employ the use of continuous soot-blowing, thus a separate PM test conducted specifically during a soot-blowing period was not necessary.

The exhaust stacks for each of boilers are 580 feet tall with an internal diameter of 28 feet. See Figure 1 for a diagram of the Unit 2 sampling location and stack dimension.

### 3.0 SAMPLING AND ANALYTICAL PROCEDURES

Emissions measurements were conducted in accordance with procedures specified in the USEPA *Standards of Performance for New Stationary Sources* or listed as an approved “*Other Test Method*”. The sampling and analytical methods used in the testing program are indicated in the table below:

Sampling Method	Parameter	Analysis
USEPA Methods 1-2	Exhaust Gas Flow Rates	Field data analysis and reduction
USEPA Method 3A	Oxygen & CO <sub>2</sub>	Instrumental Analyzer Method
USEPA Method 4	Moisture Content	Field data analysis and reduction

Sampling Method	Parameter	Analysis
USEPA Method 5B	Particulate Matter (Non-Sulfuric Acid)	Gravimetric Analysis
USEPA Method 202	PM Condensables	Gravimetric Analysis
USEPA Method 8A (NCASI Method)	Sulfuric Acid Mist/Vapor	Titration
USEPA Method 25A	Volatile Organic Compounds	Flame Ionization Detector
USEPA Method 26a	Hydrogen Chloride, Hydrogen Fluoride	Ion Chromatography
USEPA Method 29	Arsenic & Lead	As, Pb – Inductively Coupled Argon Plasma Spectroscopy
USEPA Method 30B	Total Vapor Phase Mercury Emission Concentrations	Thermal Desorption/Atomic Absorption

### 3.1 STACK GAS VELOCITY AND FLOWRATES (USEPA Methods 1-2)

#### 3.1.1 Sampling Method

Stack gas velocity traverses were conducted in accordance with the procedures outlined in USEPA Method 1, "Sample and Velocity Traverses for Stationary Sources," and Method 2, "Determination of Stack Gas Velocity and Volumetric Flowrate." During the emissions testing, four (4) sampling ports were utilized, sampling at three (3) points per port for a total of twelve (12) sampling points. Velocity traverses were conducted in conjunction with all testing method sample collection. See Figure 2 for a diagram of the traverse/sampling points used.

A cyclonic flow check was performed on the Unit 2 FGD Stack during the initial flow monitor certification RATA. Testing at all sampling locations demonstrated that no cyclonic flow was present.

#### 3.1.2 Method 2 Sampling Equipment

The EPA Method 2 sampling equipment consisted of a 0-10.0" incline manometer, S-type pitot tube ( $C_p = 0.836$ ) and a Type-K calibrated thermocouple.

## 3.2 OXYGEN AND CARBON DIOXIDE (USEPA Method 3A)

### 3.2.1 *Sampling Method*

Stack gas oxygen (O<sub>2</sub>) and carbon dioxide (CO<sub>2</sub>) emissions were evaluated using USEPA Method 3A, "Gas Analysis for Carbon Dioxide, Oxygen, Excess Air, and Dry Molecular Weight (Instrumental Analyzer Method)". The O<sub>2</sub> / CO<sub>2</sub> analyzers utilize paramagnetic sensors.

### 3.2.2 *O<sub>2</sub> / CO<sub>2</sub> Sampling Train*

The Method 3A sampling system consisted of continuously collecting a gas sample from the exhaust of the dry gas meter during each test. The sample was drawn through a Teflon<sup>®</sup> line into a Universal<sup>™</sup> gas conditioner and into a Servomex<sup>™</sup> 1400 O<sub>2</sub>/CO<sub>2</sub> gas analyzer.

### 3.2.3 *Sampling Train Calibration*

The O<sub>2</sub> / CO<sub>2</sub> analyzer was calibrated according to procedures outlined in USEPA Method 7E. Zero, span, and mid-range calibration gases were introduced directly into the analyzer to verify the instruments linearity. The O<sub>2</sub>/CO<sub>2</sub> concentrations are recorded on the field data sheets.

## 3.3 MOISTURE DETERMINATION (USEPA Method 4)

### 3.3.1 *Sampling Method*

Determination of the moisture content of the exhaust gas was performed using the method described in USEPA Method 4, "Determination of Moisture Content in Stack Gases". The exhaust gas condensate was collected in glass impingers and the percentage of moisture was derived from calculations outlined in USEPA Method 4.

## 3.4 PARTICULATE MATTER INCLUDING CONDENSABLES (USEPA Method 5B/202)

### 3.4.1 *Filterable Particulate Sampling*

USEPA Method 5B, "Determination of Non-Sulfuric Acid Particulate Matter Emissions from Stationary Sources" was used to measure the filterable (front-half) particulate emissions (see Figure 3 for a schematic of the sampling train). Triplicate, 120-minute test runs were conducted.

The Method 5B modular isokinetic stack sampling system (Figure 3) consisted of the following:

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- (1) Teflon® coated stainless-steel button-hook nozzle
- (2) Heated glass-lined probe (maintained at a temperature of  $320 \pm 25$  °F)
- (3) Heated 3" glass filter holder with a quartz filter (maintained at a temperature of  $320 \pm 25$  °F)
- (4) Set of impingers (Method 202) for the collection condensable particulates and condensate for moisture determination (see section 3.4.2, below)
- (5) Length of sample line
- (6) Environmental Supply® control case equipped with a pump, dry gas meter, and calibrated orifice.

The quartz filters used in the sampling were initially weighed to a constant weight as described in Method 5B to obtain the initial tare weight.

After completion of the final leak test for each test run, the filter was recovered, and the probe, nozzle and the front half of the filter holder assembly were brushed and rinsed with acetone. The acetone rinses were collected in a pre-cleaned sample container. The container was labeled with the test number, test location, test date, and the level of liquid marked on the outside of the container. Immediately after recovery, the sample containers were placed in a cooler for storage.

At the laboratory the acetone rinses were transferred to clean pre-weighed beakers and evaporated to dryness at ambient temperature and pressure. The beakers and filters were then placed in a desiccator for 24 hours and weighed to a constant weight (within 0.5 mg). The data sheets containing the initial and final weights of the filters and beakers can be found in Appendix C.

Collected field blanks consisted of a blank filter and acetone solution blank. The acetone blank was collected from the rinse bottle used in sample recovery. The blank filter and acetone were collected and analyzed following the same procedures used to recover and analyze the field samples.

Visible emissions (VE) readings were conducted for one hour during each Method 5B test. The VE readings were conducted according to EPA Method 9 and utilized a Certified VE person. Data sheets from the VE readings are presented in Appendix G.

Field data sheets for the Method 5B/202 sampling are in Appendix B.

### **3.4.2 Condensable Particulate Sampling Method (Method 202)**

USEPA Method 202, "Dry Impinger method for Determining Condensable Particulate Emissions from Stationary Sources" was used to measure the condensable particulate matter (CPM) (see Figure 3 for a schematic of the sampling train). This method includes procedures for measuring both organic and inorganic CPM. The Method 202

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samples were collected in conjunction with the Method 5B samples as part of the sampling train. Triplicate, 120-minute test runs were conducted.

The Method 202 impinger configuration (Figure 3) consisted of the following:

- (1) Method 23 type condenser (capable of cooling the stack gas to less than 85 °F)
- (2) Condensate dropout pot belly impinger (dry)
- (3) Modified Greenburg-Smith impinger (dry) with no taper as a backup impinger
- (4) 83mm glass filter holder with a Teflon® filter (maintained at a temperature  $\leq 85$  °F)
- (5) Modified Greenburg-Smith impinger containing 100 millimeters (ml) of distilled de-ionized (DDI) water
- (6) Modified Greenburg-Smith impinger containing approximately 300 grams of silica gel desiccant.

The condensate dropout impinger and backup impinger were placed in an insulated box with water at  $\leq 85$  °F. The water and silica gel impingers were placed in an ice water bath to maintain the exit gas temperature from the silica gel impinger below 68 °F.

All Method 202 glassware was pre-cleaned prior to testing with soap and water, and rinsed using tap water, distilled de-ionized water, and acetone. After cleaning, the glassware was baked at 300 °C for 3 hours. Prior to each sampling run, the train glassware was rinsed thoroughly with distilled de-ionized ultra-filtered water.

As soon as possible after the post-test leak check was completed, the Method 5B filter and probe were detached from the Method 202 condenser and impinger train. The Method 202 impinger train was then carefully disassembled. The liquid volume of each impinger was measured (by weight) and recorded on the field data sheet. Moisture from the condensate dropout impinger was added to the second impinger. The Method 202 impinger train was purged with ultra-high purity compressed nitrogen at 14 liters per minute for one hour. During the purge the condenser recirculation pump was operated and the first two impingers were heated/cooled to maintain the gas temperature exiting the CPM filter below 85 °F. If insufficient water was collected in the dry impinger to allow the modified insert tip to extend below the water level, 50-100 ml of de-gassed, DDI water was added to the impinger and noted on the sampling data sheet.

Contents from the dropout impinger and the impinger prior to the CPM filter were collected into a pre-cleaned sample container. The condenser, impingers and front-

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half of the CPM filter holder were rinsed with DDI water and the rinses added to the sample container. The condenser, impingers and front-half of the CPM filter holder were then rinsed with acetone followed by two rinses with Hexane. The acetone and hexane rinses were collected into a pre-cleaned sample container. The CPM filter was recovered and placed into a labeled container. All containers were labeled with the test number, test location, test date, and the level of liquid marked on the outside of the container. Immediately after recovery, the sample containers were placed in a cooler for storage.

Collected reagent blanks consisted of an acetone blank, a DDI water blank and a hexane blank taken directly from the bottles used during recovery of the samples. Additionally, a field train recovery blank was assembled and recovered following the same procedures used to prepare and recover the test samples.

Analysis of the Method 202 samples and blanks were conducted by Maxxam Analytics of Mississauga, Ontario. All analysis followed the procedures listed in Method 202. A complete laboratory report is in Appendix C.

Field data sheets for the Method 5B/202 sampling can be found in Appendix B.

### **3.4.3 Quality Control and Assurance**

All sampling and analytical equipment was calibrated according to the guidelines referenced in EPA Method 5B (see Appendix E for equipment calibration). Maxxam Analytics followed all the appropriate Method 202 analytical QA/QC (see Appendix C).

### **3.4.4 Data Reduction**

Total filterable Particulate data collected during the emissions testing was calculated and reported as pounds per hour (lbs/hr) and pounds per million Btu (lbs/MMBtu).

PM<sub>10</sub> emissions were calculated by adding the total filterable PM emissions and the condensable PM emissions. The PM<sub>10</sub> emissions were calculated and reported as pounds per hour (lbs/hr) and pounds per million Btu (lbs/MMBtu).

Emissions calculations were based on calculations located in USEPA Method 5 and Method 19. Example calculations are presented in Appendix E.

## **3.5 SULFURIC ACID MIST/VAPOR (USEPA Method 8A)**

### **3.5.1 Sulfuric Acid Mist Sampling Method**

USEPA Method 8A, "Determination of Sulfuric Acid Vapor or Mist and Sulfur Dioxide Emissions from Kraft Recovery Furnaces" (NCASI Method 8A) was used to measure the

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sulfuric acid mist emissions (see Figure 4 for a schematic of the sampling train). Method 8A uses a quartz in-line filter to remove particulate matter from the gas stream prior to capturing sulfuric acid. The use of this controlled condensation technique eliminates the potential for interference from sulfur dioxide. Triplicate, 120-minute test runs were conducted

The Method 8A stack sampling system (Figure 4) consisted of the following:

- (1) Heated quartz-lined probe (maintained at a temperature of >350 °F)
- (2) Heated glass filter holder with a quartz filter (maintained at a temperature of >500 °F)
- (3) Sulfuric acid condenser (maintained at a temperature between 167 and 185 °F)
- (4) Set of impingers for the collection of condensate
- (5) Length of sample line
- (6) Environmental Supply® control case equipped with a pump, dry gas meter, and calibrated orifice.

All sampling (non-isokinetic) was conducted at a single point in the exhaust stack. Concurrent velocity traverses were conducted during the Method 8A tests.

After completion of the final leak test for each test run, the probe was disconnected, and the system was purged with ambient air for 15 minutes at the same sampling rate recorded during the test.

Sample recovery consisted of rinsing the sulfuric acid condenser with deionized water (DI). The rinse was collected in a pre-cleaned sample container. The container was labeled with the test number, test location, test date, and the level of liquid marked on the outside of the container. Immediately following recovery, the sample container was placed in a cooler for storage.

The collected field blank was consisted of a DI rinse blank. The DI rinse blank was collected from the same bottle used in sample recovery. The DI rinse blank was collected and analyzed following the same procedures used to recover and analyze the field samples.

Analysis of the Method 8A samples and blanks were conducted by Maxxam Analytics, Mississauga, Ontario. All analysis followed the procedures listed in USEPA Method 8A. A complete laboratory report can be found in Appendix C.

Field data sheets from the Method 8A sampling are in Appendix B.

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### **3.5.2 Quality Control and Assurance**

All sampling and analytical equipment was calibrated according to the guidelines referenced in EPA Method 5 and 8A.

### **3.5.3 Data Reduction**

The H<sub>2</sub>SO<sub>4</sub> emissions data collected during the testing was calculated and reported as lbs/hr and lb/MMBtu.

## **3.6 HYDROGEN CHLORIDE, HYDROGEN FLUORIDE (USEPA Method 26A)**

### **3.6.1 HCl & HF Sampling Method**

USEPA Method 26A, "Determination of Hydrogen Halide and Halogen Emissions" (Method 26A) was used to measure the Hydrochloric Acid (HCl) and Hydrofluoric Acid (HF) emissions (see Figure 5 for a schematic of the sampling train). Method 26A uses impingers containing 0.1N H<sub>2</sub>SO<sub>4</sub> to capture the HCl & HF. Triplicate, 120-minute test runs were conducted.

The Method 26A stack sampling system (Figure 5) consisted of the following:

- (1) Teflon<sup>®</sup> coated stainless-steel button-hook nozzle
- (2) Heated glass-lined probe (Maintained >250 °F)
- (3) Heated 3" glass filter holder with a Teflon<sup>®</sup> filter (maintained at a temperature of >250 °F)
- (4) Set of impingers for the collection HCl, HF and condensate for moisture determination (Impingers containing 0.1N H<sub>2</sub>SO<sub>4</sub>)
- (5) Length of sample line
- (6) Environmental Supply<sup>®</sup> control case equipped with a pump, dry gas meter, and calibrated orifice.

All sampling was conducted isokenetically according to Method 5.

After completion of each run, a leak test was conducted. All the impingers were measured for moisture gain. Impingers 1, 2 and 3 were rinsed with H<sub>2</sub>O and their contents and associated rinses were collected in a pre-cleaned sample container. The containers were labeled with the test number, test location, test date, and the level of liquid marked on the outside of the container. Immediately after recovery, the sample containers were placed in a cooler for storage.

Collected field blanks consisted of a 0.1N H<sub>2</sub>SO<sub>4</sub> solution blank. 250ml of 0.1N H<sub>2</sub>SO<sub>4</sub> was collected and diluted with DI water, from the same bottle used in sample recovery,

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to the liquid level of the three test runs. The blank was collected and analyzed following the same procedures used to recover and analyze the field samples.

Analysis of the Method 26A samples and blanks were conducted by Maxxaam Analytics. All analysis followed the procedures listed in USEPA Method 26A. A complete laboratory report is in Appendix C.

Field data sheets for the Method 26A sampling are in Appendix B.

### **3.6.2 Quality Control and Assurance**

All sampling and analytical equipment was calibrated according to the guidelines referenced in EPA Method 5 and 26A.

### **3.6.3 Data Reduction**

The HCl and HF emissions data collected during the testing were calculated and reported as lbs/hr and lb/MMBtu.

## **3.7 ARSENIC AND LEAD (USEPA Method 29)**

### **3.7.1 Arsenic and Lead Sampling Method**

USEPA Method 29, "Determination of Metals Emissions from Stationary Sources" was used to measure the Arsenic and Lead emissions (see Figure 6 for a schematic of the sampling train). Triplicate, 120-minute test runs were conducted.

The Method 29 isokinetic stack sampling system (Figure 6) consisted of the following:

- (1) Teflon<sup>®</sup> coated stainless-steel button-hook nozzle
- (2) Heated glass-lined probe (maintained at a temperature of  $250 \pm 25$  °F)
- (3) Heated 3" glass filter holder with a quartz filter (maintained at a temperature of  $250 \pm 25$  °F)
- (4) Set of 4 impingers. Impinger 1 – empty, Impingers 2-3 containing 100 ml 5% HNO<sub>3</sub> / 10% H<sub>2</sub>O<sub>2</sub> for the collection of Arsenic, Lead, and Impinger 4 – silica gel
- (5) Length of sample line
- (6) Environmental Supply<sup>®</sup> control case equipped with a pump, dry gas meter, and calibrated orifice.

After completion of each run, the probe, filter housing and connecting glassware were rinsed with 0.1N HNO<sub>3</sub>. The filter was placed in a sealed Petri-dish. Impingers 1-3 were measured for moisture gain and their contents and associated 0.1N HNO<sub>3</sub> rinses were

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collected in a pre-cleaned sample container. Impingers 4 was measured for moisture gain.

The containers were labeled with the test number, test location, test date, and the level of liquid marked on the outside of the container. Immediately after recovery, the sample containers were placed in a cooler for storage.

Collected field blanks consisted of a blank filter and solution blanks. The DI water and solution blanks were collected from the rinse bottles used in sample recovery. The blank filter and solutions were analyzed following the same procedures used to recover and analyze the field samples.

Analysis of the Method 29 samples and blanks were conducted by Maxxam Analytics. All analysis followed the procedures listed in Method 29. A complete laboratory report is located in Appendix C.

Field data sheets for the Method 29 sampling are in Appendix B.

### ***3.7.2 Quality Control and Assurance***

All sampling and analytical equipment was calibrated according to the guidelines referenced in EPA Method 5 & 29.

### ***3.7.3 Data Reduction***

The Arsenic (As) and Lead (Pb) emissions were calculated and reported as lbs/hr and lbs/MMBtu.

## **3.8 TOTAL VAPOR PHASE MERCURY EMISSIONS (USEPA Method 30B)**

### ***3.8.1 Total Mercury Sampling Methods***

USEPA Method 30B, "Determination of Total Vapor Phase Mercury Emissions from Coal-Fired Combustion Sources Using Carbon Sorbent Traps" was used to measure the mass concentration of total vapor phase Hg in flue gas, including elemental Hg ( $Hg^0$ ) and oxidized forms of Hg ( $Hg^{+2}$ ), in micrograms per dry standard cubic meter ( $\mu g/dscm$ ) (see Figure 2 for a schematic of the sampling train). Triplicate, 60-minute test runs were conducted.

The Method 30B modular stack sampling system (Figure 8) consisted of the following:

- (1) Ohio Lumex 2-section sorbent tubes containing Iodated Activated Carbon
- (2) Heated stainless-steel probe (Containing paired sorbent traps)
- (3) Heated Teflon® sampling line (maintained at a temperature of  $250 \pm 25$  °F)

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- (4) Set of glass impingers submerged in an ice bath for the condensation and collection of moisture
- (5) Length of sample line
- (6) CleanAir™ control case equipped with duplicate pumps, dry gas meters, and calibrated orifices.

Sampling was performed at three (3) sampling points, 0.4, 1.2, and 2.0 meters, from the stack wall.

Pre- and post- leak checks were performed on the assembled sampling system. Post-leak checks are mandatory and were performed at a vacuum equal to or higher than the highest vacuum achieved during each respective test run.

At the laboratory, sorbent tube analysis was performed on an Ohio Lumex Model RA-915+ analyzer utilizing thermal desorption/atomic absorption.

The field data sheets containing the initial and final leak checks, barometric pressures, sample volumes, stack and trap temperatures and dry gas meter readings can be found in Appendix B.

### **3.8.2 Quality Control and Assurance**

Method 30B includes specific analytical QA/QC criteria that must be met in order to generate valid results. These criteria include spike recovery, sorbent trap breakthrough and paired trap agreement as described below:

- Spike recovery was determined in accordance with 30B requirements. A pre-test spike level of 30 nanograms (ng) was used. A minimum of three (3) acceptable spike recovery sample runs was obtained for Unit 2. Each of the spike recoveries must be within 85%-115% of the target.
- Sorbent trap breakthrough was determined in accordance with method 30B requirements. The Section 2 results are compared to the Section 1 results to determine the amount of breakthrough which must be  $\leq 10\%$  of the Section 1 Hg mass for Hg concentrations  $> 1$  micrograms/dry standard cubic meter (ug/dscm) or  $\leq 20\%$  of the Section 1 Hg mass for Hg concentrations  $\leq 1$  ug/dscm.
- The paired trap agreement was determined in accordance with method 30B requirements. The two (2) trap concentrations (ug/dscm) are compared for each run and must have a relative deviation (RD) of  $\leq 10\%$  for Hg concentrations  $> 1$  ug/dscm or  $\leq 20\%$  for Hg concentrations  $\leq 1$  ug/dscm.

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The analytical QA/QC data generated from the 30B samples can be found in Appendix C. The 30B sampling and analytical equipment was calibrated according to the guidelines referenced in EPA Method 30B (see Appendix D for equipment calibration).

Emissions calculations were based on calculations located in R336.1258 and USEPA Methods 30B and PS-12B. Example calculations are presented in Appendix E. Field data sheets are in Appendix B. Analytical QA/QC data are in Appendix C.

### **3.8.3 Data Reduction**

The Mercury (Hg) emissions were calculated and reported as lbs/hr and pounds per year (lb/yr).

## **3.9 VOLATILE ORGANIC COMPOUNDS (USEPA Method 25A)**

### **3.9.1 Sampling Method**

USEPA Method 25A, "Determination of Total Hydrocarbon Emissions from Stationary Sources (Instrumental Analyzer Method)" was used to measure the Volatile Organic Compounds (VOC) emissions (see Figure 7 for a schematic of the sampling train). The VOC analyzer utilizes a flame ionization detector (FID) to measure total organic hydrocarbon compounds (as propane).

The Method 25A sampling system (Figure 7) consisted of the following:

- (1) Single point sampling probe
- (2) Heated Teflon® sampling line
- (3) J.U.M.109A® Total & Non-Methane gas analyzer
- (4) Appropriate certified propane calibration gases
- (5) Data acquisition system

Sampling was conducted at a single point in the exhaust stack. Concurrent moisture (Method 4) and exhaust flow (Method 2) sampling was conducted with the VOC sampling to calculate the VOC emission rates.

### **3.9.2 Quality Control and Assurance**

In accordance with USEPA Method 25A, a 4-point (zero, low, mid, and high) calibration check was performed on the VOC analyzer. The analyzer was calibrated in the 0-50 ppm range using the following Propane (C<sub>3</sub>H<sub>8</sub>) calibration gases (0, 47.32, 25.10, and 12.97). Calibration drift checks were performed at the completion of each run and emissions data was drift corrected per USEPA Method 7E. Calibration gas certification sheets are in Appendix E.

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### **3.9.3 Data Reduction**

Data was recorded at 10-second intervals and averaged in 1-minute increments. The average VOC concentration, as Propane (C<sub>3</sub>H<sub>8</sub>) emissions were reported in parts per million (ppm), lbs/hr and lbs/MMBtu. The 1-minute readings are presented in Appendix B.

## **4.0 OPERATING PARAMETERS**

The test program included the collection of boiler operating data, CEMs emission data, precipitator operating data, SCR operating data, sulfur control system operating data, and FGD scrubber operating data during each emission test.

During each day of emissions sampling, a representative coal sample was collected from the unit and analyzed for ultimate and proximate analysis, including % Sulfur, % Ash, and heat content.

CEMs data, operational data and control equipment data collected during the testing are presented in Appendix F. Results from the coal analysis are in Appendix F.

## **5.0 DISCUSSION OF RESULTS**

Table 1 presents the Particulate Matter (PM) emission testing results and the Condensable Particulate emissions testing results. Particulate emissions are presented in pounds per hour (lbs/hr) and pounds per Million British thermal units (lbs/MMBtu). Unit 2 has a Permit Limit for PM less than 10 microns (PM<sub>10</sub>). PM<sub>10</sub> cannot be measured per Method 201 because of the FGD and potential water droplets in the exhaust gas, therefore all PM measured (Method 5B and 202) were combined to represent the PM<sub>10</sub> emissions. The average total filterable PM emissions of 0.010 lbs/MMBtu were below the permit limit of 0.011 lbs/MMBtu. The average PM<sub>10</sub> emissions of 0.013 lbs/MMBtu were less than the permit limit of 0.024 lbs/MMBtu.

Table 2 presents the Sulfuric Acid (H<sub>2</sub>SO<sub>4</sub>) emission testing results. The H<sub>2</sub>SO<sub>4</sub> emissions are presented in pounds per hour (lbs/hr) and pounds per Million British thermal units (lbs/MMBtu). All tests were reported as less than "<" since the analytical results were all below the reportable detection limit. The average H<sub>2</sub>SO<sub>4</sub> emissions of <0.001 lbs/MMBtu were below the permit limit of 0.005 lbs/MMBtu.

Table 3 presents the Hydrogen Chloride (HCl) and Hydrogen Fluoride (HF) emission testing results. The HCl and HF emissions are presented in pounds per hour (lbs/hr) and pounds per Million British thermal units (lbs/MMBtu). The average HCl emissions of 0.0004 lbs/MMBtu were below the permit limit of 0.0024 lbs/MMBtu. All HF tests were reported as less than "<"

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since the analytical results were all below the reportable detection limit. The average HF emissions of <0.00010 lbs/MMBtu were below the permit limit of 0.00023 lbs/MMBtu.

Table 4 presents the Lead (Pb) and Arsenic (As) emission testing results. The Lead and Arsenic emissions are presented in pounds per hour (lbs/hr) and pounds per Million British thermal units (lbs/MMBtu). The average Lead emissions of 0.004 lbs/hr and 0.0000006 lbs/MMBtu were below the permit limits of 0.13 lbs/hr and 0.0000169 lbs/MMBtu. The average Arsenic emissions of 0.0000007 lbs/MMBtu were below the permit limit of 0.0000063 lbs/MMBtu.

Table 5 presents the Mercury (Hg) emission testing results. The Mercury emissions are presented in lbs/hr and pounds per year (lbs/yr). The average Hg emissions of 24.7 lbs/yr were below the permit limit of 143.1 lbs/yr.

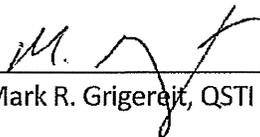
Table 6 presents the Volatile Organic Compound (VOC) emission testing results. The VOC emissions are presented in parts per million (ppm), pounds per hour (lbs/hr) and pounds per Million British thermal units (lbs/MMBtu), all as propane. The average VOC emissions of <1.4 lbs/hr and <0.0002 lbs/MMBtu were below the permit limits of 25.9 lbs/hr and 0.0034 lbs/MMBtu.

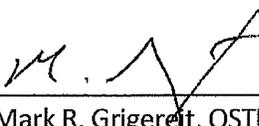
The Auxiliary test data presented in each Table for each test includes the Unit Load in gross megawatts (GMW), stack temperature in degrees Fahrenheit (°F), stack gas moisture in percent (%), stack gas velocity in feet per minute (ft/min), and stack gas flow rate in actual cubic feet per minute (ACFM), standard cubic feet per minute (SCFM) and dry standard cubic feet per minute (DSCFM).

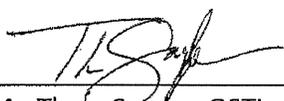


6.0 CERTIFICATION STATEMENT

"I certify that I believe the information provided in this document is true, accurate, and complete. Results of testing are based on the good faith application of sound professional judgment, using techniques, factors, or standards approved by the Local, State, or Federal Governing body, or generally accepted in the trade."

  
\_\_\_\_\_  
Mark R. Grigereit, QSTI

This report prepared by:   
\_\_\_\_\_  
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This report reviewed by:   
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Mr. Thom Snyder, QSTI  
Environmental Specialist, Environmental Field Services  
Environmental Management and Resources  
DTE Energy Corporate Services, LLC

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## RESULTS TABLES



**TABLE NO. 1**  
**TOTAL PARTICULATE & CONDENSABLE PARTICULATE EMISSION TESTING RESULTS**  
**Monroe Power Plant - Unit 2 FGD Stack**  
**June 17, 2019**

Test	Test Date	Test Time	Unit Load (GMW)	Stack Temperature (°F)	Stack Moisture (%)	Stack Velocity (ft/min)	Exhaust Gas Flowrates			PM Emissions		PM <sub>10</sub> Emissions		Visible Emissions <sup>(3)</sup> (%)
							(ACFM)	(SCFM)	(DSCFM)	(lbs/hr)	(lbs/MMBtu) <sup>(1)</sup>	(lbs/hr)	(lbs/MMBtu) <sup>(2)</sup>	
PM-1	17-Jun-19	6:24-8:30	749.7	124.9	14.7	3,845	2,367,701	2,069,715	1,766,315	52.02	0.007	71.53	0.010	0
PM-2	17-Jun-19	8:51-11:00	749.8	125.3	14.7	3,834	2,360,855	2,062,262	1,759,060	87.31	0.012	102.51	0.014	0
PM-3	17-Jun-19	11:22-13:32	<u>749.4</u>	<u>125.2</u>	<u>14.6</u>	<u>3,841</u>	<u>2,365,379</u>	<u>2,066,802</u>	<u>1,765,772</u>	<u>71.57</u>	<u>0.010</u>	<u>101.74</u>	<u>0.014</u>	<u>0</u>
<b>Average:</b>			<b>749.6</b>	<b>125.1</b>	<b>14.6</b>	<b>3,840</b>	<b>2,364,645</b>	<b>2,066,260</b>	<b>1,763,716</b>	<b>70.30</b>	<b>0.010</b>	<b>91.93</b>	<b>0.013</b>	<b>0</b>

(1) Permit Limit = 0.011 lb/MMBtu

(2) Permit Limit = 0.024 lb/MMBtu

(3) Permit Limit = 10%



**TABLE NO. 2**  
**Sulfuric Acid (H<sub>2</sub>SO<sub>4</sub>) EMISSION TESTING RESULTS**  
**Monroe Power Plant - Unit 2 FGD Stack**  
**June 19, 2019**

Test	Test Date	Test Time	Unit Load (GMW)	Stack Temperature (°F)	Stack Moisture (%)	Stack Velocity (ft/min)	Exhaust Gas Flowrates			Sulfuric Acid (H <sub>2</sub> SO <sub>4</sub> ) Emissions	
							(ACFM)	(SCFM)	(DSCFM)	(lbs/hr)	(lbs/MMBtu) <sup>(1)</sup>
H <sub>2</sub> SO <sub>4</sub> -1	19-Jun-19	6:49-8:49	748.3	126.0	15.0	3,781	2,328,118	2,063,805	1,754,328	<3.43	<0.0005
H <sub>2</sub> SO <sub>4</sub> -2	19-Jun-19	9:23-10:23	753.5	125.9	14.8	3,763	2,317,011	2,054,251	1,751,197	<6.83	<0.0009
H <sub>2</sub> SO <sub>4</sub> -3	19-Jun-19	11:02-12:02	<u>753.3</u>	<u>126.0</u>	<u>14.8</u>	<u>3,800</u>	<u>2,339,680</u>	<u>2,074,055</u>	<u>1,767,028</u>	<u>&lt;7.59</u>	<u>&lt;0.0010</u>
<i>Average:</i>			<i>751.7</i>	<i>126.0</i>	<i>14.9</i>	<i>3,781</i>	<i>2,328,270</i>	<i>2,064,037</i>	<i>1,757,518</i>	<i>5.95</i>	<i>0.0008</i>

(1) Permit Limit = 0.005 lb/MMBtu



**TABLE NO. 3**  
**HYDROGEN CHLORIDE (HCl) & HYDROGEN FLUORIDE (HF) EMISSION TESTING RESULTS**  
 Monroe Power Plant - Unit 2 FGD Stack  
 June 19, 2019

Test	Test Date	Test Time	Unit Load (GMW)	Stack Temperature (°F)	Stack Moisture (%)	Stack Velocity (ft/min)	Exhaust Gas Flowrates			Hydrogen Chloride (HCl) Emissions		Hydrogen Fluoride (HF) Emissions	
							(ACFM)	(SCFM)	(DSCFM)	(lbs/hr)	(lbs/MMBtu) <sup>(1)</sup>	(lbs/hr)	(lbs/MMBtu) <sup>(2)</sup>
HCl-1	19-Jun-19	6:32-8:41	748.3	126.0	15.0	3,781	2,328,118	2,063,805	1,754,328	2.67	0.0004	<0.74	<0.00010
HCl-2	19-Jun-19	8:57-11:05	753.5	125.9	14.8	3,763	2,317,011	2,054,251	1,751,197	2.71	0.0004	<0.74	<0.00010
HCl-3	19-Jun-19	11:16-13:22	<u>753.3</u>	<u>126.0</u>	<u>14.8</u>	<u>3,800</u>	<u>2,339,680</u>	<u>2,074,055</u>	<u>1,767,028</u>	<u>3.87</u>	<u>0.0005</u>	<u>&lt;0.74</u>	<u>&lt;0.00010</u>
<b>Average:</b>			<b>751.7</b>	<b>126.0</b>	<b>14.9</b>	<b>3,781</b>	<b>2,328,270</b>	<b>2,064,037</b>	<b>1,757,518</b>	<b>3.08</b>	<b>0.0004</b>	<b>&lt;0.74</b>	<b>&lt;0.00010</b>

(1) Permit Limit = 0.0024 lb/MMBtu

(2) Permit Limit = 0.00023 lb/MMBtu



**TABLE NO. 4**  
**LEAD (Pb) and ARSENIC (As) EMISSION TESTING RESULTS**  
**Monroe Power Plant - Unit 2 FGD Stack**  
**June 18, 2019**

Test	Test Date	Test Time	Unit Load (GMW)	Stack Temperature (°F)	Stack Moisture (%)	Stack Velocity (ft/min)	Exhaust Gas Flowrates			Lead Emissions		Arsenic Emissions	
							(ACFM)	(SCFM)	(DSCFM)	(lbs/hr) <sup>(1)</sup>	(lbs/MMBtu) <sup>(1)</sup>	(lbs/hr)	(lbs/MMBtu) <sup>(2)</sup>
M29-1	18-Jun-19	6:07-8:15	753.7	125.4	15.2	3,844	2,366,707	2,068,161	1,753,901	0.005	0.0000007	0.005	0.0000007
M29-2	18-Jun-19	8:34-10:40	753.2	125.7	15.1	3,883	2,390,709	2,088,244	1,772,546	0.004	0.0000006	0.005	0.0000007
M29-3	18-Jun-19	11:00-13:06	753.6	126.1	15.2	3,818	2,350,834	2,051,954	1,740,939	0.004	0.0000005	0.005	0.0000007
<i>Average:</i>			753.5	125.7	15.2	3,848	2,369,417	2,069,453	1,755,795	0.004	0.0000006	0.005	0.0000007

(1) Permit Limit = 0.13 lb/hr & 0.0000169 lb/MMBtu

(2) Permit Limit = 0.0000063 lb/MMBtu



**TABLE NO. 5**  
**MERCURY (Hg) EMISSION TESTING RESULTS**  
**Monroe Power Plant - Unit 2 FGD Stack**  
**June 17 & 18, 2019**

Test	Test Time	Unit Load (GMW)	Stack Temperature (°F)	Stack Moisture (%)	Stack Velocity (ft/min)	Exhaust Gas Flowrates			Mercury Emissions	
						(ACFM)	(SCFM)	(DSCFM)	(lbs/hr)	(lbs/yr) <sup>(1)</sup>
M30B-1	12:29-13:29	749.4	125.2	14.7	3,841	2,365,379	2,066,802	1,765,772	0.003	28.97
M30B-2	6:12-7:12	753.7	125.4	15.2	3,844	2,366,707	2,068,161	1,753,901	0.003	23.54
M30B-3	9:06-10:06	753.2	<u>125.7</u>	<u>15.1</u>	<u>3,883</u>	<u>2,390,709</u>	<u>2,088,244</u>	<u>1,772,546</u>	<u>0.002</u>	<u>21.58</u>
			<b>125.4</b>	<b>15.0</b>	<b>3,856</b>	<b>2,374,265</b>	<b>2,074,402</b>	<b>1,764,073</b>	<b>0.003</b>	<b>24.70</b>

(1) Permit Limit = 143.1 lb/yr



**TABLE NO. 6**  
**VOLATILE ORGANIC COMPOUND (VOC) EMISSION TESTING RESULTS**  
**Monroe Power Plant - Unit 2 FGD Stack**  
**June 17, 2019**

Test	Test Date	Test Time	Unit Load (GMW)	Stack Temperature (°F)	Stack Moisture (%)	Stack Velocity (ft/min)	Exhaust Gas Flowrates			VOC Emissions (as propane)		
							(ACFM)	(SCFM)	(DSCFM)	(ppm) <sup>(2)</sup>	(lbs/hr) <sup>(1)</sup>	(lbs/MMBtu) <sup>(1)</sup>
VOC-1	17-Jun-19	6:58-7:58	749.7	124.9	14.7	3,845	2,367,701	2,069,715	1,766,315	<0.1	<1.4	<0.0002
VOC-2	17-Jun-19	9:24-10:24	749.8	125.3	14.7	3,834	2,360,855	2,062,262	1,759,060	<0.1	<1.4	<0.0002
VOC-3	17-Jun-19	11:22-12:22	<u>749.4</u>	<u>125.2</u>	<u>14.6</u>	<u>3,841</u>	<u>2,365,379</u>	<u>2,066,802</u>	<u>1,765,772</u>	<u>&lt;0.1</u>	<u>&lt;1.4</u>	<u>&lt;0.0002</u>
<i>Average:</i>			<i>749.6</i>	<i>125.1</i>	<i>14.6</i>	<i>3,840</i>	<i>2,364,645</i>	<i>2,066,260</i>	<i>1,763,716</i>	<i>&lt;0.1</i>	<i>&lt;1.4</i>	<i>&lt;0.0002</i>

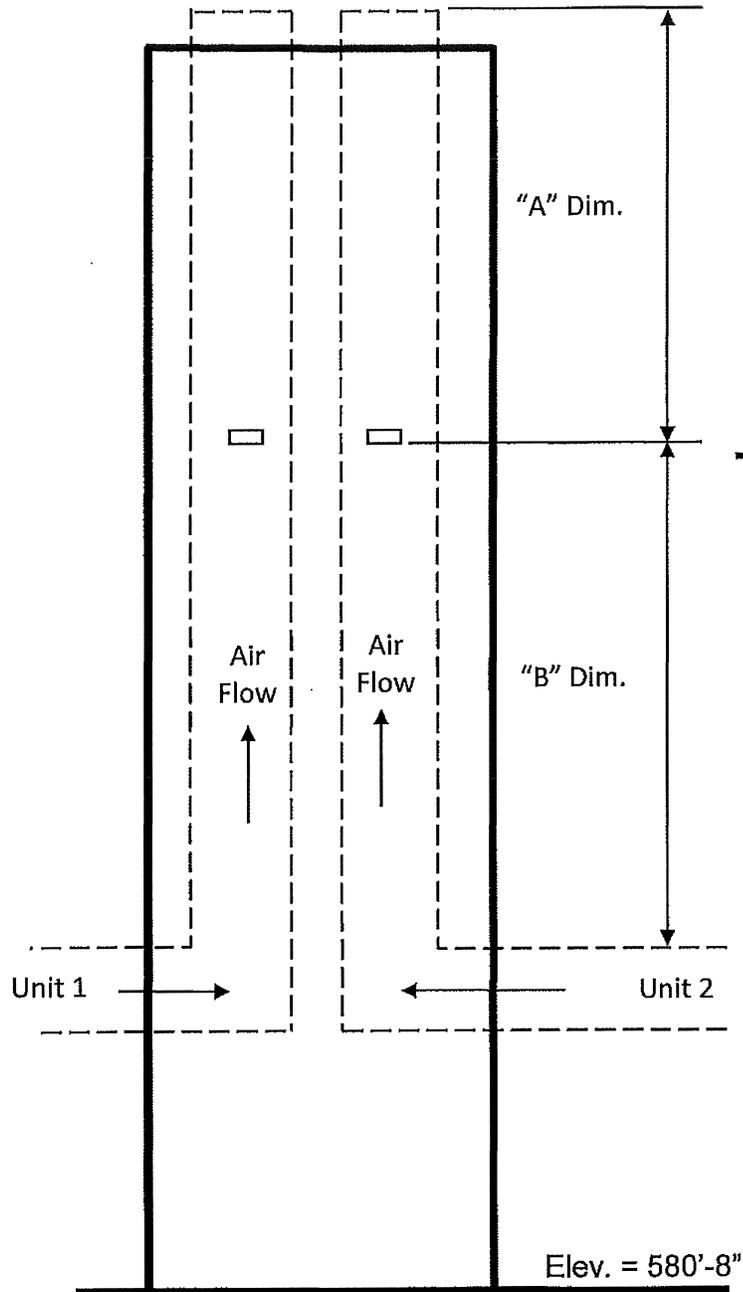
(1) Permit Limit = 25.9 lb/hr & 0.0034 lb/MMBtu

(2) Corrected for analyzer drift as per USEPA Method 7E, Emission BDL 0.1 ppm

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**FIGURES**

Figure 1 – Sampling Location  
Monroe Power Plant – Units 1-2  
June 17-19, 2019



**Details**

"A" Dim = Upstream Distance

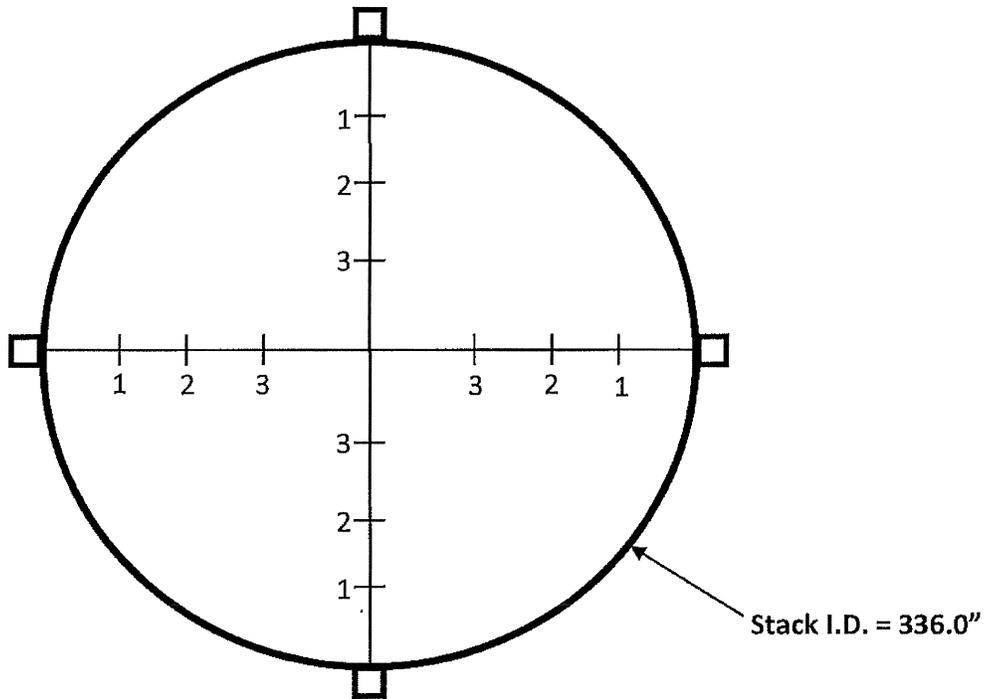
"A" Dim = 201.6'

"B" Dim = Downstream Distance

"B" Dim = 233.8'

Dia. @ Sample Location = 28'-0"

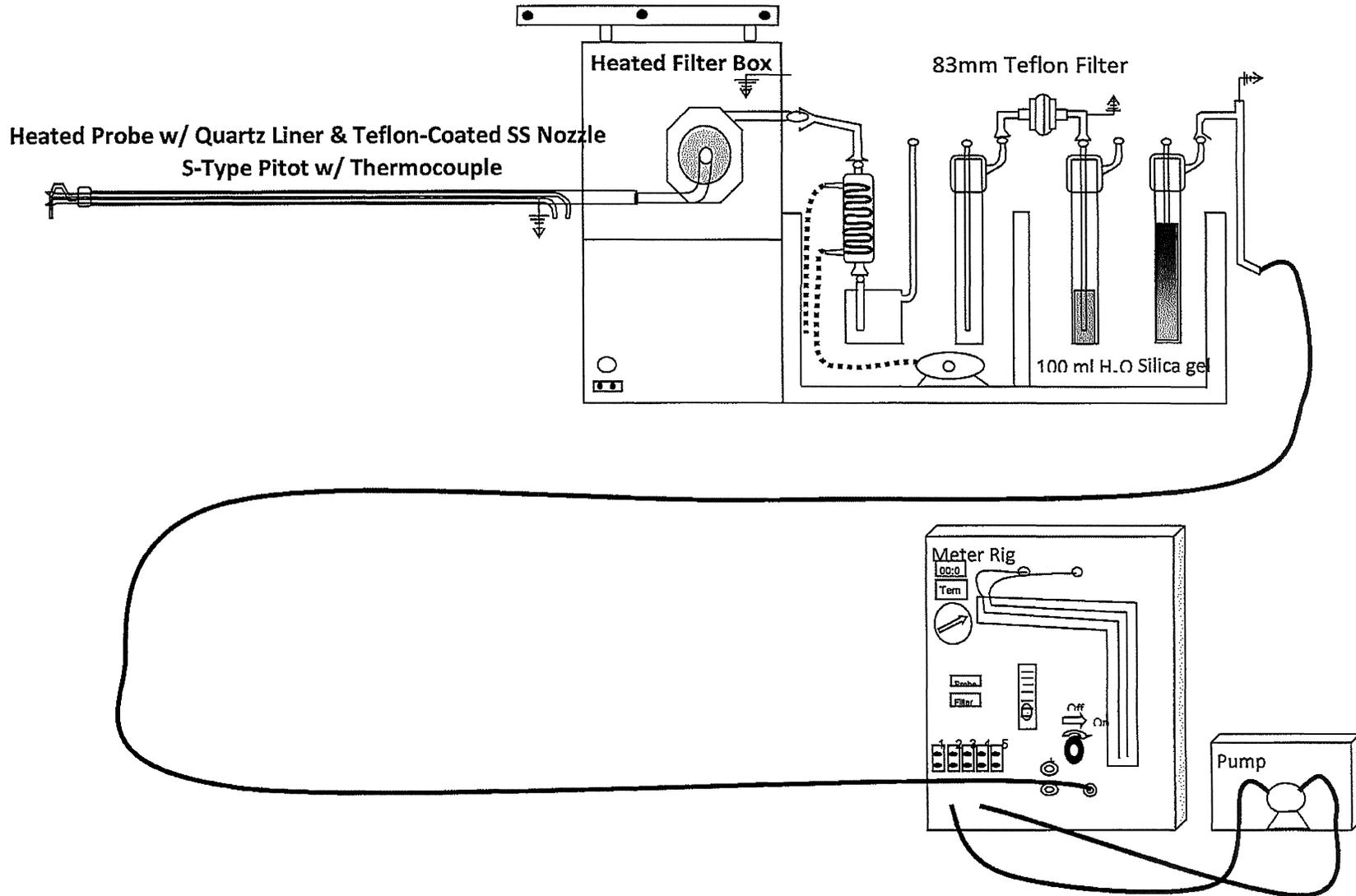
Figure 2 – Sampling Points  
Monroe Power Plant – Units 1-2  
June 17-19, 2019



VELOCITY / MEASUREMENT  
POINTS

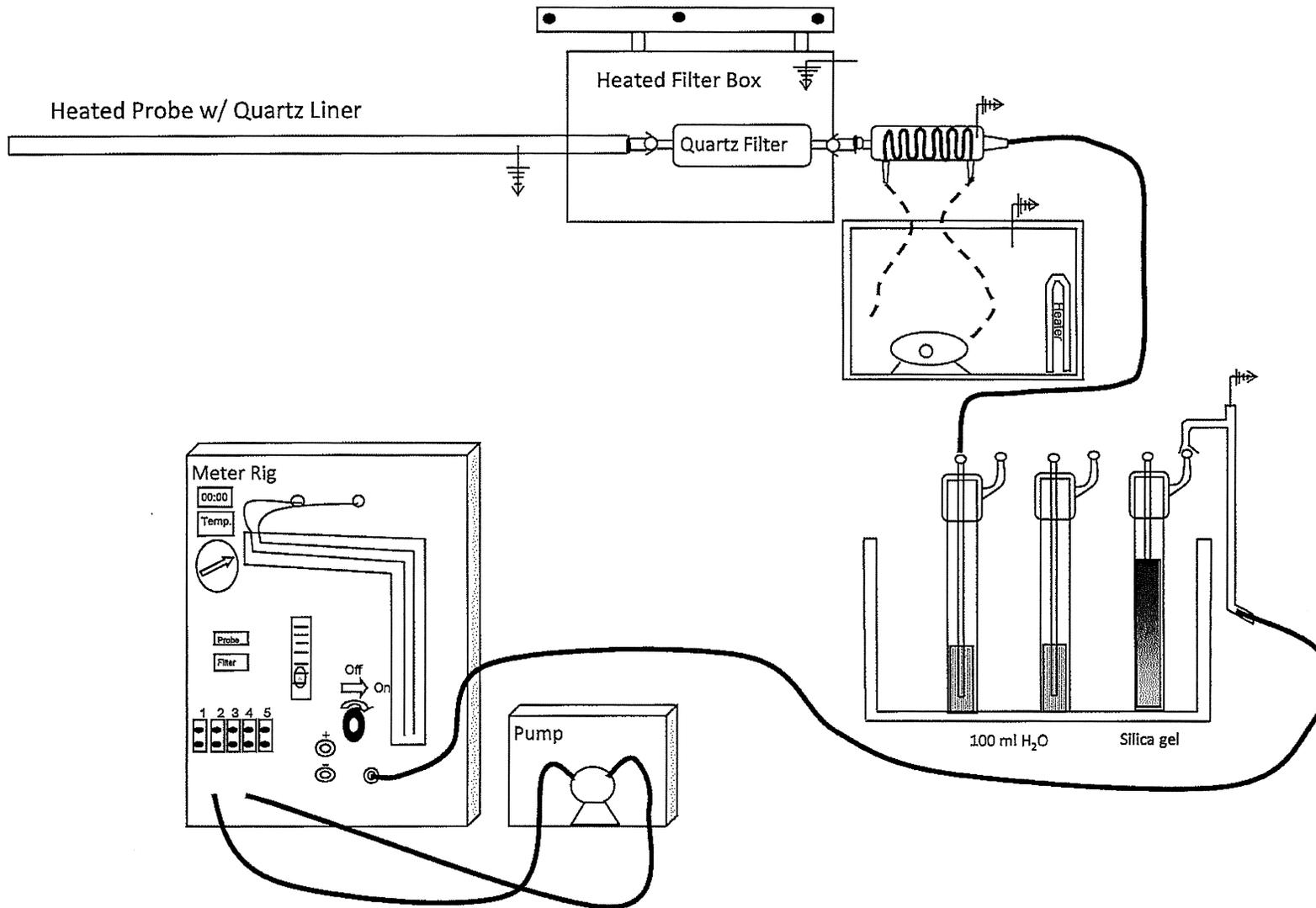
Point	Distance from Inside Wall
1	14.78"
2	49.06"
3	99.46"

Figure 3 – EPA Method 5B / 202  
Monroe Power Plant – Units 1-2  
June 17-19, 2019



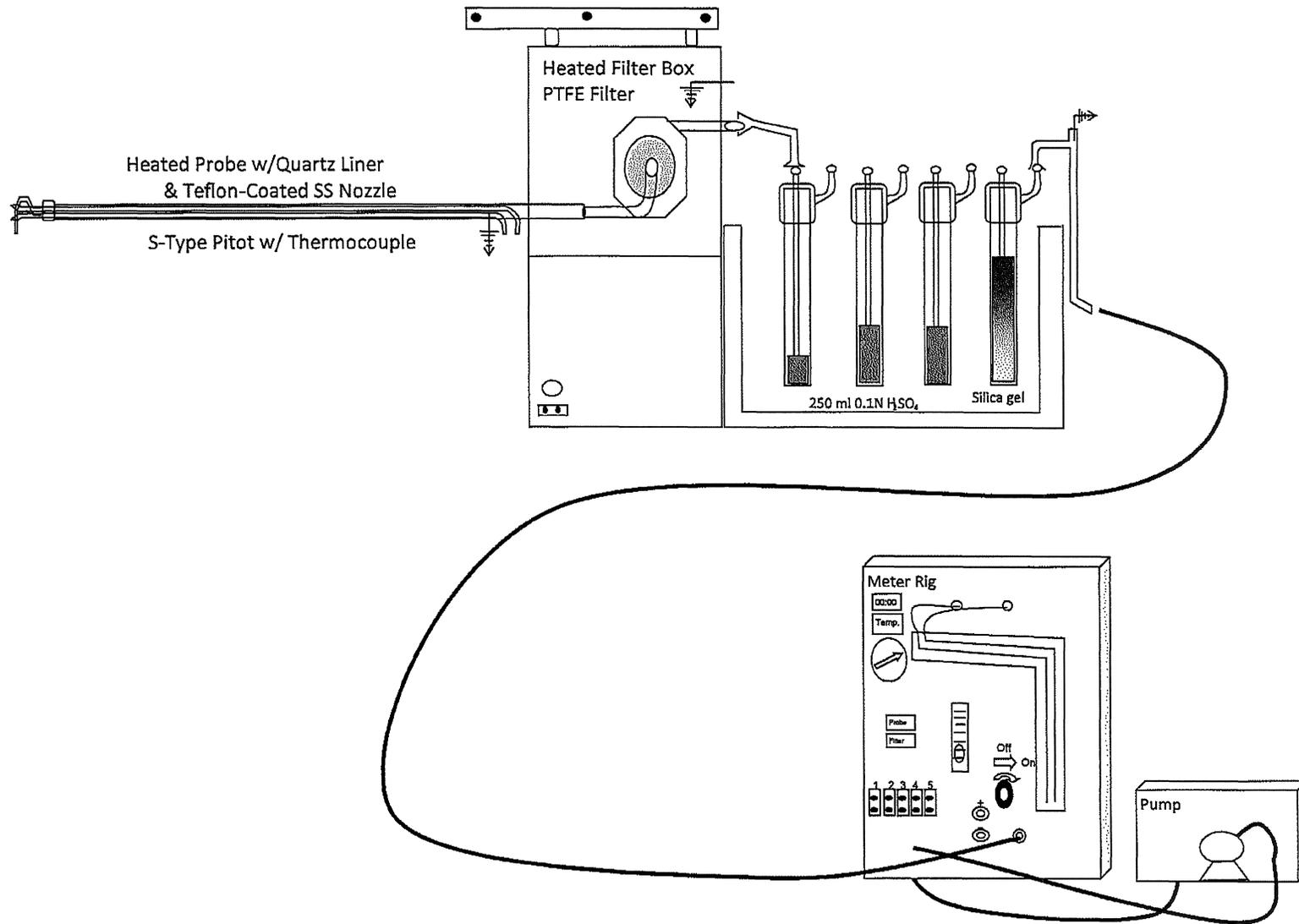
**DTE**

Figure 4 – EPA Method 8A  
Monroe Power Plant – Units 1-2  
June 17-19, 2019



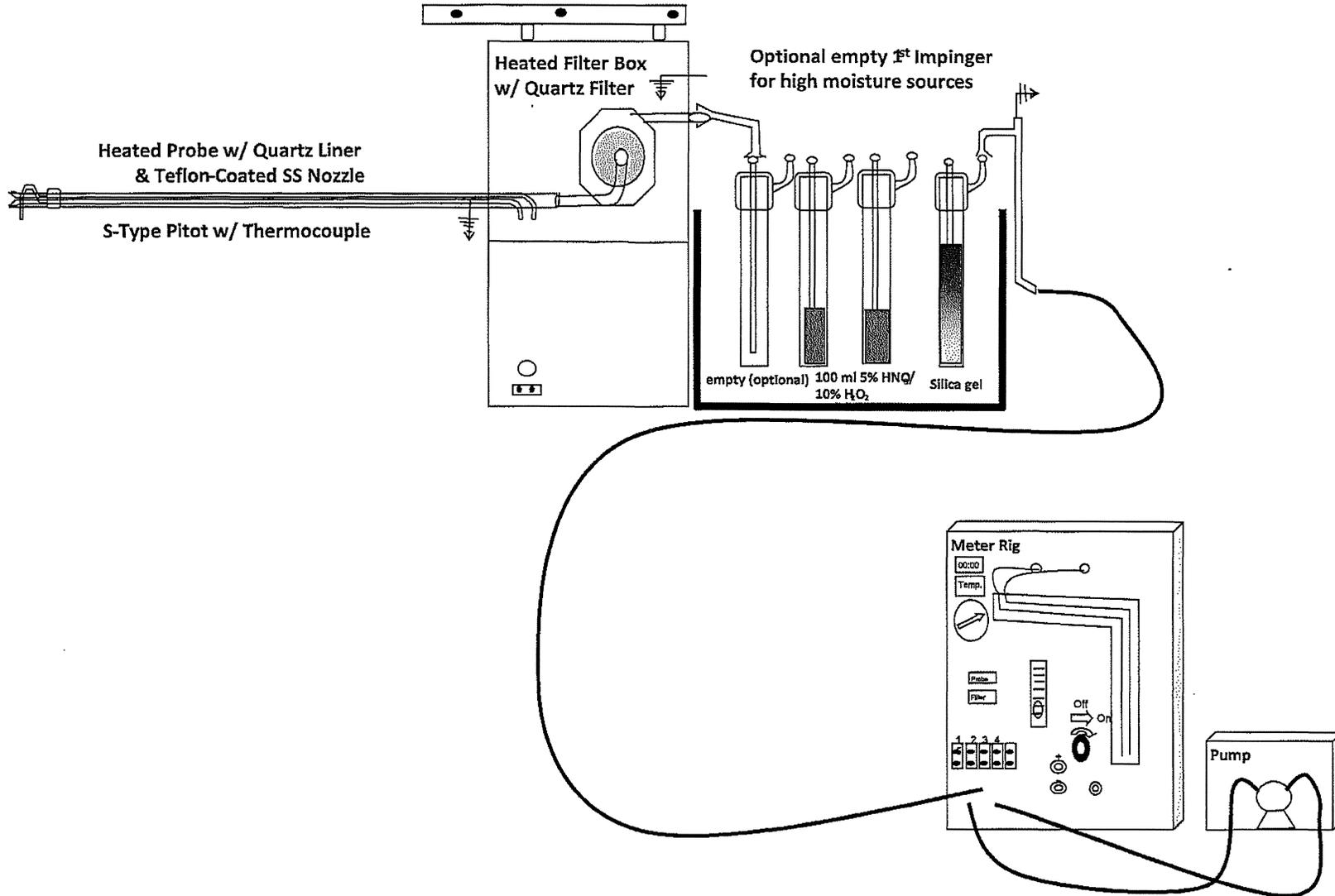
**DTE**

Figure 5 – EPA Method 26A  
Monroe Power Plant – Units 1-2  
June 17-19, 2019



**DTE**

Figure 6 – EPA Method 29  
Monroe Power Plant – Units 1-2  
June 17-19, 2019



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Figure 7 – EPA Method 25A  
Monroe Power Plant – Units 1-2  
June 17-19, 2019

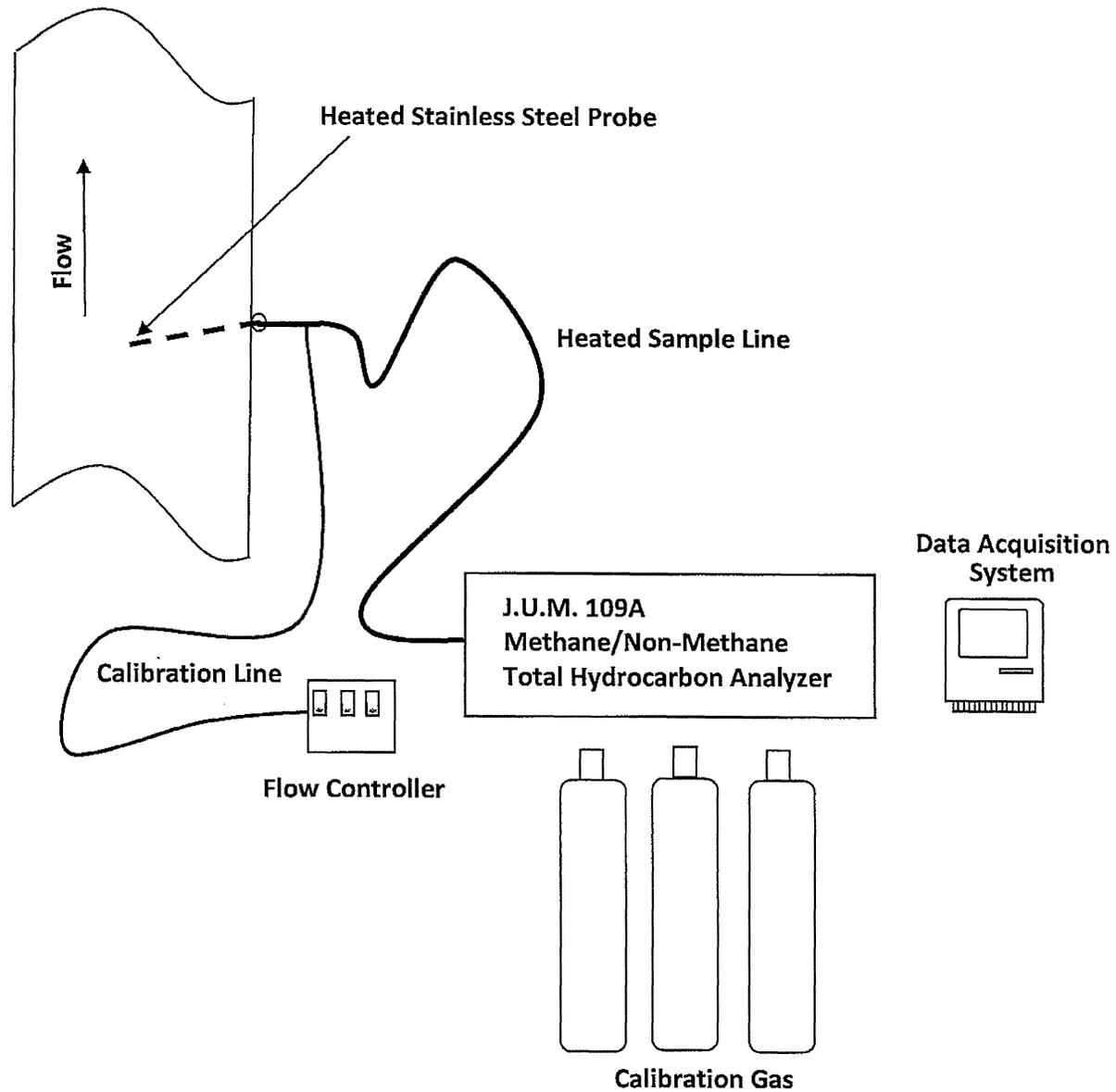


Figure 8 – EPA Method 30B  
Monroe Power Plant – Units 1-2  
June 17-19, 2019

