

#### EMISSIONS COMPLIANCE STUDY

Performed At The Carmeuse Lime, Inc. River Rouge Facility Kilns 1 and 2 River Rouge, Michigan

Test Date October 31, 2023

Report No. TRC Environmental Corporation Report 555553

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#### **Report Certification**

I certify that to the best of my knowledge:

- Testing data and all corresponding information have been checked for accuracy and completeness.
- Sampling and analysis have been conducted in accordance with the approved protocol and applicable reference methods (as applicable).
- All deviations, method modifications, or sampling and analytical anomalies are summarized in the appropriate report narrative(s).

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Craig L.Grunden, QI Project Manager

December 6, 2023 Date

TRC was operating in conformance with the requirements of ASTM D7036-04 during this test program.

Bruce Randall TRC Emission Testing Technical Director



### **Table of Contents**

1.0 INTRODUCTION	. 4
1.1 Project Contact Information	. 4
1.2 Facility and Process Description	. 5
2.0 SUMMARY OF RESULTS	. 5
3.0 DISCUSSION OF RESULTS	. 6
4.0 SAMPLING AND ANALYSIS PROCEDURES	. 6
4.1 Determination of Sample Point Locations by USEPA Method 1	. 7
4.2 Volumetric Flow Rate Determination by USEPA Method 2	. 7
4.3 Determination of the Concentration of Gaseous Pollutants Using a Multi-Pollutant Sampling	
System	
4.3.1 CO2 Determination by USEPA Method 3A	
4.3.2 O2 Determination by USEPA Method 3A	. 8
4.3.3 SO <sub>2</sub> Determination by USEPA Method 6C	. 8
4.4 Moisture Determination by USEPA Method 4	. 8
4.5 Filterable PM Determination by USEPA Method 5	. 8
4.6 Condensable PM Determination by USEPA Method 202	
4.7 Visible Emissions Determination by USEPA Method 9	. 9
4.8 Determination of SO <sub>2</sub> Removal Efficiency and PM, SO <sub>2</sub> and NO <sub>x</sub> Emission Rates by USEPA Method	
19	. 9
5.0 QUALITY ASSURANCE PROCEDURES	10
6.0 TEST RESULTS SUMMARY	11

#### APPENDIX

AETB and QI Information Summary
Qualified Individual Certificate(s)
Process and Pollution Control Equipment Operating Data
Sample Location Information
Sample Analysis Data
Calculation Nomenclature and Formulas
Processed Field Data and Results
Processed Visible Emission Data
Visible Emission Observer Certificate
Sampling Equipment Calibration Data
Response Time Data
Analyzer Interference Test Data
Calibration Gas Certificates
Raw Field Data Sheets
Test Protocol



#### EMISSIONS COMPLIANCE STUDY

#### **1.0 INTRODUCTION**

TRC Environmental Corporation (TRC) performed an emissions compliance test program on Kilns 1 and 2 at the River Rouge Facility of Carmeuse Lime, Inc. (Carmeuse) in River Rouge, Michigan on October 31, 2023. The tests were authorized by - and performed for Carmeuse Lime, Inc.

The purpose of this test program was to determine total particulate matter (TPM), particulate matter less than 10 microns (PM<sub>10</sub>), particulate matter less than 2.5 microns (PM<sub>2.5</sub>), condensable particulate matter (CPM), sulfur dioxide (SO<sub>2</sub>) and Visible Emissions (VE) on Kilns 1 and 2 combined exhaust during normal operating conditions. The results of the test program will be used in order to determine compliance with Michigan Department of Environmental Quality (MDEQ) The test program was conducted according to the TRC Test Protocol dated July 19, 2023.

Test Facility	Carmeuse Lime, Inc. River Rouge Facility 25 Marion Ave River Rouge, Michigan 48218 Permit No. 128-17 Facility No. B2169	Raymond Rummel Area Environmental Manager (219) 292-5206 (phone) raymond.rummel@carmeuse.com
Air Emissions Testing Body (AETB)	TRC Environmental Corporation 2500 Eldo Road Monroeville, Pennsylvania 15146	Craig L. Grunden, QI Project Manager (412) 925-0066 (phone) (844) 625-4557 (fax) CGrunden@TRCCompanies.com

#### 1.1 Project Contact Information

The tests were conducted by Aaron M. Blum, QI, Gavin Lewis, Andrew J. Stapfer and M. Beck Heil of TRC. Documentation of the on-site ASTM D7036-04 Qualified Individual(s) (QI) can be located in the appendix to this report.

Steve Weiss from the MDEQ was present to observe the testing.



#### 1.2 Facility and Process Description

Lime is the product of the high-temperature calcination of limestone. The basic procedures in the production of lime are (1) quarrying the raw limestone, (2) preparing the limestone for the kilns by crushing and sizing, (3) calcining the limestone to quicklime (CaO) and (4) miscellaneous transfer, storage, and handling operations.

Carmeuse operates two rotary kilns at their River Rouge facility. Emissions from Rotary Kilns 1 and 2 each duct into a combined stack after separate fabric filter baghouse control devices. Coal is used as the fuel for both kilns.

#### 2.0 SUMMARY OF RESULTS

The results of this test program are summarized in the table below. Detailed individual run results are presented in Section 6.0.

Unit ID	Emission Point	Pollutant Tested	Emissions Result	Emission Limit
		FPM <sup>3</sup>	0.004 lb/tsf 1	0.12 lb/tsf <sup>1</sup>
		VE	0% over a 6-minute average	15% over a 6-minute average
EUKILNNUMBER1 Combined and Exhaust EUKILNNUMBER2 Stack	Combined	SO <sub>2</sub>	193.23 ppm in exhaust to gas (corrected to 50% excess O <sub>2</sub> )	300 ppm in exhaust to gas (corrected to 50% excess O <sub>2</sub> )
			155 lb/hr	470 lb/hr
		0.441 lb/MMBtu <sup>2</sup>	2.4 lb/MMBtu <sup>2</sup>	
		PM <sub>10</sub> <sup>3</sup>	1.73 lb/hr	23.45 lb/hr
		PM <sub>2.5</sub> <sup>3</sup>	1.73 lb/hr	23.45 lb/hr

<sup>1</sup>Pounds per ton of stone feed

<sup>2</sup> Pounds per million BTU

<sup>3</sup> All PM collected in the M5/202 train were considered less than PM2.5 and used to comply with the PM/PM10/PM2.5 limits



The table below summarizes the test methods used, as well as the number and duration of each at each test location:

Unit ID/ Sample Location	Parameter Measured	USEPA Test Method	No. of Runs	Run Duration (Mins)
	Sample / Velocity Traverses	1		
EUKILNNUMBER1 and EUKILNNUMBER2 Combined Exhaust Stack	Velocity – S-type Pitot	2		NA
	O <sub>2</sub> , CO <sub>2</sub>	3A		
	Moisture Content	4		
	Particulate Matter <sup>4</sup>	5 and 202	3	
	SO <sub>2</sub>	6C		60
	VE	9		
	Fuel Flow Emission Rates	19		

<sup>4</sup> All PM collected in the M5/202 train were considered less than PM2.5 and used to comply with the PM/PM10/PM2.5 limits

#### 3.0 DISCUSSION OF RESULTS

No problems were encountered with the testing equipment during the test program. Source operation appeared normal during the entire test program. No changes or problems were encountered that required modification of any procedures presented in the test plan. No adverse test or environmental conditions were encountered during the conduct of this test program.

#### 4.0 SAMPLING AND ANALYSIS PROCEDURES

All testing, sampling, analytical, and calibration procedures used for this test program were performed in accordance with the methods presented in the following sections. Where applicable, the Quality Assurance Handbook for Air Pollution Measurement Systems, Volume III, Stationary Source Specific Methods, USEPA 600/R-94/038c, September 1994 was used to supplement procedures.



#### 4.1 Determination of Sample Point Locations by USEPA Method 1

This method is applicable to gas streams flowing in ducts, stacks, and flues and is designed to provide guidance for the selection of sampling ports and traverse points at which sampling for air pollutants will be performed. Sample ports must be located at least two duct diameters downstream and a half a duct diameter upstream from any flow disturbance.

The cross-section of the measurement site was divided into a number of equal areas, and the traverse points were located in the center of each area. The minimum number of points were determined from Figure 1-1 (particulate) of the Method.

#### 4.2 Volumetric Flow Rate Determination by USEPA Method 2

This method is applicable for the determination of the average velocity and the volumetric flow rate of a gas stream.

The gas velocity head ( $\Delta P$ ) and temperature were measured at traverse points defined by USEPA Method 1. The velocity head was measured with a Type S (Stausscheibe or reverse type) pitot tube and oil-filled manometer; and the gas temperature was measured with a Type K thermocouple. The average gas velocity in the flue was calculated based on: the gas density (as determined by USEPA Methods 3A and 4); the flue gas pressure; the average of the square roots of the velocity heads at each traverse point, and the average flue gas temperature.

#### 4.3 Determination of the Concentration of Gaseous Pollutants Using a Multi-Pollutant Sampling System

Concentrations of the pollutants in the following sub-sections were determined using one sampling system. The number of points at which sample was collected was determined in accordance with Method 7E specifications.

A straight-extractive sampling system was used. A data logger continuously recorded pollutant concentrations and generated one-minute averages of those concentrations. All calibrations and system checks were conducted using USEPA Protocol gases. A calibration gas dilution system certified in accordance with USEPA Method 205 was used to dilute USEPA Protocol gases to generate the required calibration concentrations. Three-point linearity checks were performed prior to sampling, and in the event of a failing system bias or drift test (and subsequent corrective action). System bias and drift checks were performed using the low-level gas and either the high- or mid-level gas (as specified in the appendices) prior to and following each test run.

Analyzer interference tests were conducted in accordance with the regulations in effect at the time that TRC placed an analyzer model in service.



#### 4.3.1 CO<sub>2</sub> Determination by USEPA Method 3A

This method is applicable for the determination of  $CO_2$  concentrations in controlled and uncontrolled emissions from stationary sources only when specified within the regulations. The  $CO_2$  analyzer was equipped with a non-dispersive infrared (IR) detector.

#### 4.3.2 O<sub>2</sub> Determination by USEPA Method 3A

This method is applicable for the determination of  $O_2$  concentrations in controlled and uncontrolled emissions from stationary sources only when specified within the regulations. The  $O_2$  analyzer was equipped with a paramagnetic-based detector.

#### 4.3.3 SO<sub>2</sub> Determination by USEPA Method 6C

This method is applicable for the determination of  $SO_2$  concentrations in controlled and uncontrolled emissions from stationary sources only when specified within the regulations. The  $SO_2$  analyzer was equipped with an ultraviolet (UV) detector.

#### 4.4 Moisture Determination by USEPA Method 4

This method is applicable for the determination of the moisture content of stack gas.

A gas sample was extracted at a constant rate from the source. Moisture was removed from the sample stream by a series of pre-weighed impingers immersed in an ice bath. A minimum of 21 dry standard cubic feet of flue gas was collected during each sample run.

#### 4.5 Filterable PM Determination by USEPA Method 5

This method is applicable for the determination of PM emissions from stationary sources. USEPA Methods 2-4 were performed concurrently with, and as an integral part of, these determinations.

Flue gas was withdrawn isokinetically from the source at traverse points determined per USEPA Method 1, and PM was collected in the nozzle, probe liner, and on a glass fiber filter. The probe liner and filter were maintained at a temperature of  $120\pm14^{\circ}C$  (248 +/-25°F) or the temperature specified in the test protocol. The PM mass, which included any material that condensed at or above the filtration temperature, was determined gravimetrically after the removal of uncombined water.

#### 4.6 Condensable PM Determination by USEPA Method 202

This method is applicable for the determination of condensable particulate matter (CPM) from stationary sources. CPM is measured in the emissions after removal from the stack and after passing thRouge a filter.



The CPM was collected in dry impingers after filterable particulate material had been collected on filters maintained above 30°C (85°F) using the previously identified Method. The CPM sample train included a Method 23 type condenser capable of cooling the stack gas to less than 85°F, followed by a water dropout impinger. One modified Greenburg Smith impinger and a CPM filter followed the water dropout impinger. Prior to recovery, the impinger contents were immediately purged after the run with nitrogen (N<sub>2</sub>) to remove dissolved sulfur dioxide. The impinger solution was then extracted with hexane, and the CPM filter was extracted with water and hexane. The organic and aqueous fractions were then taken to dryness and the residues weighed. A correction, if necessary, was made for any ammonia present due to laboratory analysis procedures. The total of all fractions represented the CPM.

#### 4.7 Visible Emissions Determination by USEPA Method 9

This method is applicable for the determination of the opacity of emissions from stationary sources pursuant to § 60.11(b) and for visually determining opacity of emissions.

Opacity observations were made by a qualified observer. Observations were made at the point of greatest opacity in the portion of the plume where condensed water vapor was not present. Observations were made at 15-second intervals for the duration of the test period.

# 4.8 Determination of $SO_2$ Removal Efficiency and PM, $SO_2$ and $NO_x$ Emission Rates by USEPA Method 19

Where specified by an applicable subpart of the regulations, this method is applicable for the determination of (a) PM, SO<sub>2</sub>, and NO<sub>x</sub> emission rates; (b) sulfur removal efficiencies of fuel pretreatment and SO<sub>2</sub> control devices; and (c) overall reduction of potential SO<sub>2</sub> emissions.

Emission Rates. Oxygen  $(O_2)$  or carbon dioxide  $(CO_2)$  concentrations and appropriate F factors (ratios of combustion gas volumes to heat inputs) were used to calculate pollutant emission rates from pollutant concentrations.

Sulfur Reduction Efficiency and SO<sub>2</sub> Removal Efficiency. An overall SO<sub>2</sub> emission reduction efficiency was computed from the efficiency of fuel pretreatment systems, where applicable, and the efficiency of SO<sub>2</sub> control devices. The sulfur removal efficiency of a fuel pretreatment system was determined by fuel sampling and analysis of the sulfur and heat contents of the fuel before and after the pretreatment system. The SO<sub>2</sub> removal efficiency of a control device was determined by measuring the SO<sub>2</sub> rates before and after the control device.



#### **5.0 QUALITY ASSURANCE PROCEDURES**

TRC integrates our Quality Management System (QMS) into every aspect of our testing service. We follow the procedures specified in current published versions of the test Method(s) referenced in this report. Any modifications or deviations are specifically identified in the body of the report. We routinely participate in independent, third-party audits of our activities, and maintain:

- Accreditation from the Louisiana Environmental Laboratory Accreditation Program (LELAP);
- Accreditation from the Stack Testing Accreditation Council (STAC) and the American Association for Laboratory Accreditation (A2LA) that our operations conform with the requirements of ASTM D 7036 as an Air Emission Testing Body (AETB).

These accreditations demonstrate that our systems for training, equipment maintenance and calibration, document control and project management will fully ensure that project objectives are achieved in a timely and efficient manner with a strict commitment to quality.

All calibrations are performed in accordance with the test Method(s) identified in this report. If a Method allows for more than one calibration approach, or if approved alternatives are available, the calibration documentation in the appendices specifies which approach was used. All measurement devices are calibrated or verified at set intervals against standards traceable to the National Institute of Standards and Technology (NIST). NIST traceability information is available upon request.

ASTM D7036-04 specifies that "AETBs shall have and shall apply procedures for estimating the uncertainty of measurement. Conformance with this section may be demonstrated by the use of approved test protocols for all tests. When such protocols are used, reference shall be made to published literature, when available, where estimates of uncertainty for test methods may be found." TRC conforms with this section by using approved test protocols for all tests. 555553 - Carmeuse Lime Inc - River Rouge Kilns 1 and 2 Emissions Compliance Test Report



#### **6.0 TEST RESULTS SUMMARY**



Page 1 of 1

#### PARTICULATE TEST RESULTS SUMMARY

 Company:
 Carmeuse

 Plant:
 River Rouge

 Unit:
 Kilns 1 & 2

 Location:
 Outlet

Test Run Number:	Run 1	2	3	Average
Source Condition:	MNOC	MNOC	MNOC	
Date:	10/31/2023	10/31/2023	10/31/2023	
Start Time:	10:42	13:00	15:15	
End Time:	12:20	14:15	16:50	
Sample Duration (min):	60.0	60.0	60.0	60.0
Average Gas Temp, T <sub>s</sub> , (°F):	368.3	367.3	371.0	368.9
Fractional Gas Moisture Content, Bws:	0.080	0.080	0.085	0.082
Gas O <sub>2</sub> Content (%vol):	8.6	9.0	9.1	8.9
Gas Wet MW, M <sub>s</sub> , (lb/lb-mole):	30.15	30.06	29.99	30.07
Average Gas Velocity, V <sub>s</sub> , (ft/sec):	45.10	43.88	46.09	45.03
Measured Volumetric Flow Rate:				
Q (actual ft <sup>3</sup> /min):	172,159	167,501	175,942	171,867
Q <sub>std</sub> (std ft <sup>3</sup> /min):	107,466	104,695	109,250	107,137
Q <sub>std(dry)</sub> (dry std ft <sup>3</sup> /min):	98,839	96,285	100,009	98,378
Process Rate (ton stone feed/hr):	80.70	80.57	79.78	80.35
Sample Volume, V <sub>m(std)</sub> , (dry std ft <sup>3</sup> ):	48.850	47.193	49.403	48.482
PM Collected, (mg):				
Filterable, m <sub>n</sub> :	0.30	2.90	0.30	1.17
Condensable, m <sub>cpm</sub> :	2.50	6.50	6.80	5.27
Total, m <sub>total</sub> :	2.80	9.40	7.10	6.43
PM Concentration, (gr/dscf):				
Filterable, Cs:	0.0001	0.0009	0.0001	0.0004
Condensable, C <sub>cpm</sub> :	0.0008	0.0021	0.0021	0.0017
Total, C:	0.0009	0.0031	0.0022	0.0021
PM Emission Rate, ER <sub>M2</sub> , (lb/hr based on me	easured volumetric flow	w rate):		
Filterable:	0.08	0.78	0.08	0.31
Condensable:	0.67	1.75	1.82	1.41
Total:	0.75	2.54	1.90	1.73
PM Emission Rate, ER, (lb/process rate):	(lb/ton stone feed	)		
Filterable:	0.001	0.010	0.001	0.004
Condensable:	0.008	0.022	0.023	0.018
Total:	0.009	0.031	0.024	0.022
Isokinetic Variance, I:	100.0	99.1	99.9	99.7

## TRC

#### Instrumental Reference Method Calibration Corrected Test Data

Project Number:	555553	Start Date:	10/31/23
Customer:	Carmeuse	End Date:	10/31/23
Unit Identification:	Kilns 1 & 2	Facility:	River Rouge
Sample Location:	Outlet	Recorded by:	Aaron M. Blum, QI
Load Level/Condition:	MNOC	Fd Factor:	Varies

Run #	Date	Start Time	End Time	NOX ppmvd	SO2 ppmvd	CO	CO2 % v/v dry	02 % v/v dry
1	10/31/23	10:42	11:41		185.0	-	17.9	8.6
2	10/31/23	13:00	13:59	-	167.4	-	17.2	9.0
3	10/31/23	15:06	16:05	-	121.1		17.1	9.1
Average				-	157.85	-	17.39	8.92

Reference Method Results, CEM Moisture Basis								
Run #	NOX ppmvd	SO2 ppmvd	CO ppmvd	CO2 % v/v dry	O2 % v/v dry	Bws	Fc Factor	Fd Factor
1	-	185.0	-	17.9	8.6	0.080		9672
2	-	167.4	-	17.2	9.0	0.080		9662
3	-	121.1	-	17.1	9.1	0.085		9682
Average		157.85		17.39	8.92	0.082		9672

Run #	NOX Ib/MMBtu	SO2 Ib/MMBtu	CO Ib/MMBtu	NOX lb/hr	SO2 lb/hr	CO Ib/hr	Flow DSCFM
1	-	0.505	-	-	182.67	-	99112
2		0.473	-	54	160.52	-	96285
3	-	0.346	-		120.65		100009
Average		0.441	-	-	154.613	-	98,468.7

	Test Calculation S ed Using Ib/MMBtu		or and Heat Inpu	ıt
Run #	Heat Input MMBtu/Hr	NO <sub>x</sub> lb/hr	SO <sub>2</sub> Ib/hr	CO Ib/hr
1	361.98	-	183	
2	339.62	-2	161	
3	348.86	-	121	16
Average	350.2	•	155	-

Run #	Heat Input MMBtu/Hr	NOX Ib/MMBtu	SO2 Ib/MMBtu	CO Ib/MMBtu
1	362.0	-	0.505	-
2	339.6	-	0.473	
3	348.9	-	0.346	-
Average	350,152	-	0.441	141

Customer: Unit ID: Sample Loc:		Carmeuse Kilns 1 & 2 Outlet			River Rouge	
Use?					RM	
1 = Y	Test		Start	End	SO <sub>2</sub>	
0 = N	Run	Date	Time	Time	ppm corrected to 50% excess air	
0	1	10/31/2023	10:42	11:41	221.07	
0	2	10/31/2023	13:00	13:59	207.27	
0	3	10/31/2023	15:06	16:05	151.34	
Average:					193.23	
	•					

### Sulfur Dioxide (SO<sub>2</sub>), ppm corrected to 50% excess air