Nitrogen Oxides Emissions Testing of Boiler No. 3

Nexteer Automotive 3900 Holland Road Saginaw, Michigan

State Registration No. A6175 Permit to Install 99-13a

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Prepared for Nexteer Automotive Saginaw, Michigan

Bureau Veritas Project No. 11014-000059.00 April 24, 2014



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## **Executive Summary**

Nexteer Automotive retained Bureau Veritas North America, Inc. to test air emissions from the Boiler No. 3 exhaust at its facility in Saginaw, Michigan. The testing was performed in order to satisfy testing requirements and evaluate compliance with emission limits in Michigan Department of Environmental Quality Permit to Install 99-13a for the Boiler No. 3 source.

Air emissions testing consisted of measuring the following parameters:

- Flue gas velocity, molecular weight, and moisture content
- Concentration of oxygen (% O<sub>2</sub>)
- Concentration of oxides of nitrogen (parts per million NO<sub>x</sub>)

Bureau Veritas tested the following source:

• Boiler No. 3 150 million British thermal unit per hour (MMBtu/hr) heat input naturalgas-fired boiler that supplies 125,000 pound per hour (lb/hr) of process steam to the facility

On April 9, 2014, air emission testing was performed following United States Environmental Protection Agency (USEPA) Methods 1 through 4, 7E, and 19 and State of Michigan Part 10 Rules at the outlet of the boiler. The air emission testing was conducted as described in the Intent-to-Test plan submitted to MDEQ on March 10, 2014, and approved by MDEQ on March 11, 2014.

The results of the testing are summarized in the table on the following page. Detailed results are presented in Table 1 in the appendix of this report.



#### Natural Gas-Fired Boiler No. 3

Parameter	Units	Run 1	Run 2	Run 3	Average	Permit Limit†		
Steam Production	kpph	115.8	115.9	115.5	115.7	N/A		
Natural Gas Use	Mcf/hr	132	119	115	122	N/A		
%O <sub>2</sub> Trim Setting	%	50.5	50.5	50.5	50.5	N/A		
$NO_x$ concentration <sup>‡</sup>	ppmvd	76.9	78.8	76.7	77.5	N/A		
$O_2$ concentration <sup>‡</sup>	%	2.5	2.5	2.5	2.5	N/A		
NO <sub>x</sub> Mass Emission Rate	lb/MMBtu	0.091	0.093	0.091	0.091	0.11		
NO <sub>x</sub> Mass Emission Rate	lb/hr	16.0	17.1	16.8	16.6	17		

#### **Boiler No. 3 Emission Results**

<sup>1</sup> concentration corrected for analyzer drift per USEPA Method 7E, equation 7E-5b Kpph = thousand pound per hour
 Mcf/hr = thousand cubic foot per hour
 ppmvd = part per million by volume, dry basis

The results of this test program indicate Boiler No. 3 at the Nexteer Automotive facility is operating in compliance with permit limits.



## **1.0 Introduction**

Nexteer Automotive retained Bureau Veritas North America, Inc. to test air emissions from Boiler No. 3 exhaust at its facility in Saginaw, Michigan. The testing was performed in order to satisfy testing requirements and evaluate compliance with emission limits in Michigan Department of Environmental Quality Permit to Install 99-13a for the Boiler No. 3 source.

Air emissions testing consisted of measuring the following parameters:

- Flue gas velocity, molecular weight, and moisture content
- Concentration of oxygen (% O<sub>2</sub>)
- Concentration of oxides of nitrogen (parts per million NO<sub>x</sub>)

Bureau Veritas tested the following source:

• Boiler No. 3 150 million British thermal unit per hour (MMBtu/hr) heat input naturalgas-fired boiler that supplies 125,000 pound per hour (lb/hr) of process steam to the facility

The air emission testing was conducted on April 9, 2014 as described in the Intent-to-Test plan submitted to MDEQ on March 10, 2014, and approved by MDEQ on March 11, 2014.

#### 1.1 Identification, Location, and Dates of Test

The testing was performed at the Nexteer Automotive facility on April 9, 2014. The source, parameters, and test dates are presented in the following table:

Source Identification, Parameters, and Dates of Tests						
Source Identification	Parameter	Test Date				
Boiler No. 3 – EUBR03	NO <sub>x</sub> , O <sub>2</sub>	April 9, 2014				
NO <sub>x</sub> : oxides of nitrogen O <sub>2</sub> : oxygen						

Table 1-1Source Identification, Parameters, and Dates of Tests



## **1.2** Purpose of Testing

The purpose of the testing was to satisfy testing requirements and evaluate compliance with emission limits in Michigan Department of Environmental Quality Permit to Install 99-13a for the Boiler No. 3 source.

## 1.3 Description of Source

The source tested generates hot water and steam for distribution to the automotive manufacturing complex. The following table describes the source tested.

Emission Unit ID	Emission Unit Description	Flexible Group ID
EUBR03 (Boiler No. 3)	Hot water is generated for plant use using a natural gas boiler. The boiler has a rated heat input of 150 million British thermal units (MMBtu) and can supply 125,000 pounds per hour (lb/hr) of process steam to the plant.	Not applicable

Table 1-2Description of Source

Figure 1 (after the Figures Tab in the Appendix) depicts the exhaust ductwork and sampling locations.

The boiler exhaust is located on the roof of the powerhouse building. The stack is 66 inches in diameter where it exhausts to atmosphere. Sampling ports are installed in accordance with USEPA Method 1 guidelines. The sampling ports are accessible via a ladder and a platform on the stack. A photograph of the source is presented in Figure 1-1.



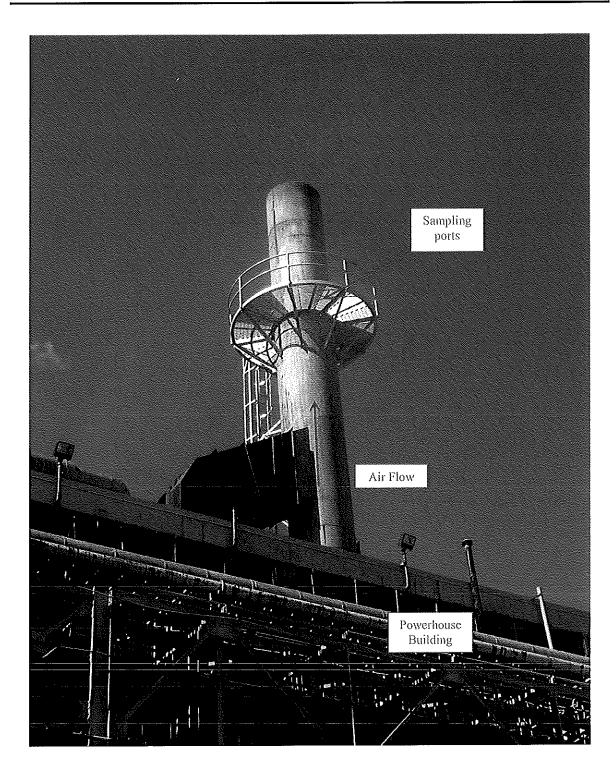


Figure 1-1. Boiler No. 3 Exhaust



Two 4-inch-internal-diameter sampling ports, oriented at 90° to one another, were used for sampling. The sampling ports extend 6 inches outward from the stack interior wall. The sampling ports are located at the following locations relative to the nearest flow disturbances:

- Approximately 18 feet downstream of a duct confluence (~3.3 stack diameters)
- Approximately 11.5 feet upstream of the stack's exhaust to atmosphere (~2.1 stack diameters)

### **1.4 Contact Information**

Mr. Thomas Schmelter, Senior Project Manager with Bureau Veritas, directed the compliance testing program. Mr. Dominic DeCarlo, Facilities and Environmental Engineer, and Ms. Kim Bostek, Supervisor and Environmental Engineer, with Nexteer Automotive, provided process coordination and arranged for facility operating parameters to be recorded.

Mr. Nathan Hude and Mr. Ben Witkopp with Michigan Department of Environmental Quality witnessed the testing. Mr. Witkopp is the state inspector assigned to the facility. Contact information for these individuals is listed in Table 1-3 on the following page.



#### Table 1-3 Contact Information

Nexteer Automotive				
Dominic DeCarlo	Kim Bostek			
Facilities and Environmental Engineer	Supervisor, Environmental Engineer			
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Regulatory Agency				
Nathan Hude	Ben Witkopp			
Michigan Dept. of Environmental Quality	Michigan Dept. of Environmental Quality			
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huden@michigan.gov	witkoppb@michigan.gov			



## 2.0 Summary of Results

## 2.1 Operating Data

Nexteer Automotive personnel recorded operating parameters during the emissions testing. The following operating data were recorded:

- Natural gas use (cubic foot per hour)
- Boiler load as steam output (lb/hour)
- Boiler %O<sub>2</sub> Trim Setting

Mr. Hude with MDEQ verified that the operating parameters were recorded appropriately. The recorded operating parameters are included in Appendix E and summarized in Table 2-1.

Testing Parameter	Run	Sampling Time	Steam Output (kpph)	Natural Gas Use (standard cubic feet per hour)	Boiler %O <sub>2</sub> Trim Setting
	1	10:45-11:45	115.8	132,000	50.5
NO	2	12:00-13:00	115.9	119,000	50.5
NO <sub>x</sub>	3	13:10-14:10	115.5	115,000	50.5
		Average	115.7	122,000	50.5

Table 2-1April 9, 2014, Boiler No. 3 Operating Parameters

Operating parameters were averaged over the duration of each test run.

## 2.2 Applicable Permit or Source Designation

The applicable permit is Michigan Department of Environmental Quality Permit to Install 99-13a.

## 2.3 Comparison to Emission Regulations

The permit requires testing to evaluate compliance with the following emission limits within 60 days after achieving maximum production rate, but not later than 180 days after commencement of initial start-up. The results are used to evaluate compliance with the facility's emission limits for  $NO_x$ . The relevant emission limits in the permit are presented in Table 2-2.



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# Table 2-2Emission Limits

Source	Oxides of Nitrogen Emission Limit
Boiler 3 – EUBR03	0.11 lb NO <sub>x</sub> /MMBtu
	17 lb NO <sub>x</sub> /hr

The results of the testing are compared to permit limits in Table 2-3. Detailed results are presented in Table 1 after the Tables tab in the Appendix. Graphs of measured oxygen and oxides of nitrogen concentrations are provided after the Graphs tab.

#### Natural Gas-Fired Boiler No. 3

Parameter	Units	Run 1	Run 2	Run 3	Average	Permit Limit'
Steam Production	kpph	115.8	115.9	115.5	115.7	N/A
Natural Gas Use	Mcf/hr	132	119	115	122	N/A
%O <sub>2</sub> Trim Setting	%	50.5	50.5	50.5	50.5	N/A
NO <sub>x</sub> Concentration	ppmvd	76.9	78.8	76.7	77.5	N/A
O <sub>2</sub> Concentration	%	2.5	2.5	2.5	2.5	N/A
NO <sub>x</sub> Mass Emission Rate	lb/MMBtu	0.091	0.093	0.091	0.091	0.11
NO <sub>x</sub> Mass Emission Rate	lb/hr	16.0	17.1	16.8	16.6	in sang Sang
<sup>†</sup> : Limit is expressed as the a kpph: thousand pound per he sef/hr: standard cubic foot per Mcf/hr = thousand cubic foo ppmvd: part per million by v	our er hour t per hour	st runs.			•	

**Boiler No. 3 Emission Results** 

The results of this test program indicate Boiler No. 3 at the Nexteer Automotive facility is operating in compliance with permit limits.



## **3.0 Source Description**

### 3.1 **Process Description**

Nexteer Automotive is a designer and manufacturer of steering columns, shafts, integral steering gears, rack and pinion steering gears, power steering pumps, advanced steering systems and complete steering modules with anti-theft features for various vehicle manufacturers. Operations are conducted in six buildings and a powerhouse on the property.

The powerhouse was built in 1952 and operates three coal-fired boilers (Boiler No. 1 is no longer in operation) and two natural-gas-fired boilers to generate process and heating steam for use throughout the complex. Boiler No. 3 is a natural-gas-fired boiler with a maximum heat input capacity of 150 mmBtu. The powerhouse has the capacity to generate a maximum of 460,000 pounds per hour (pph) of steam.

Boilers 4, 5, and 6 are underthrow stoker coal-fired that have a maximum heat input capacity of 220 million British thermal units per hour (mmBtu/hr). Soot blows are performed on average once per day on the boiler(s) in operation. The soot blows are typically 45 minutes in duration and assist in the cleaning of the tubes in the convective back pass and air pre-heater. Boiler No. 2 is a natural-gas-fired boiler with a maximum heat input capacity of 77 mmBtu.

Boiler No. 3 was recently converted from a coal-fired boiler to a 150,000 mmBtu/hr natural gas fired boiler. Emissions from this source are generated through the combustion of natural-gas using low oxides of nitrogen (NO<sub>x</sub>) burners and are vented through exhaust stack SV-BR03 exiting the roof of the powerhouse building.

## 3.2 Process Flow

Combustion air mixes with natural gas at the burner in Boiler No. 3. The energy from combustion heats the water wall tubes and steam drum. Flue gas from the furnace is exhausted using an induction fan that creates negative pressure within the combustion chamber. The flue gas is directed through a heat exchanger (economizer) before exhausting to atmosphere.

The combustion heats water wall tubes and the upper steam drum. The water wall tubes transfer water between the mud drum and the upper steam drum. The mud drum contains water and is indirectly heated by the furnace. The upper steam drum, directly heated by the furnace, captures steam and directs it to the common header pipe where the steam is distributed at approximately 135 pounds per square inch throughout the facility. The steam condensate is returned to the powerhouse.

Up to 90% of the water/steam generated by the boilers returns to the powerhouse and is directed to a water storage holding vessel in the basement of the powerhouse. From the holding vessel,



the water is directed to a deaerated feed tank where tap water is added to compensate for the distribution loss. Corrosion inhibitors and pH balancing chemicals are added prior to the water from the deaerated tank being introduced into the boiler steam drum.

## 3.3 Materials Processed During Tests

The materials processed during the test were water and natural gas. Water is monitored as steam produced (measured in pounds of steam per hour). Natural gas was monitored in cubic feet per hour. These data were recorded by Nexteer Automotive personnel and are summarized in Section 2.1.

Prior to initiating a test run, Bureau Veritas coordinated with Nexteer Automotive, which verified the process was operating in accordance with designated specifications. Recorded operating data are included in Appendix E.

## 3.4 Rated Capacity of Process

The capacity of the boiler is based on its heat input rating. The operating capacity of the boiler is based on steam demand and the amount of steam pressure in the steam distribution piping. The rated capacity of the No. 3 boiler, as noted in the applicable permit, is presented in the following table:

7	Table 3-1				
Rated Capacity of No. 3 Boiler					
Boiler	Boiler Rated Capacity				

Boiler	Rated Capacity (mmBtu/hr)
3	150

mmBtu/hr: million British thermal unit per hour



## 4.0 Sampling and Analytical Procedures

Bureau Veritas measured emissions in accordance with the procedures specified in the USEPA Standards of Performance for New Stationary Sources and State of Michigan Part 10 Rules Intermittent Testing and Sampling. The sampling and analytical methods used are indicated in the Table 4-1:

Sampling Method	Parameter	Analysis
USEPA 1 and 2	Gas stream volumetric flowrate	Field measurement, S-type Pitot tube
USEPA 3	Molecular weight	Fyrite® chemical absorbance analyzer
USEPA 3A	Molecular weight	Instrument infrared analysis
USEPA 4	Moisture content	Gravimetric
USEPA 7E	Nitrogen oxide concentration	Chemiluminescence
USEPA 19	Nitrogen oxide emission rates	Ratio of combustion gas volume to heat input

Table 4-1Emission Test Methods

## 4.1 Sampling Train and Procedures

The emissions test parameters and sampling procedures are presented in Table 4-2.

 Table 4-2

 Sampling and Analytical Methods

	Source	Reference Method			
Parameter	Boiler No. 3 Method	Title			
Sampling ports and traverse points	•	USEPA 1	Sample and Velocity Traverses for Stationary Sources		
Velocity and flowrate	•	USEPA 2	Determination of Stack Gas Velocity and Volumetric Flow Rate (Type S Pitot Tube)		
Molecular weight	•	USEPA 3	Gas Analysis for the Determination of Dry Molecular Weight		



**Reference** Method Source Boiler Parameter No. 3 Method Title **USEPA 3A** Determination of Oxygen and Carbon Dioxide Concentrations in Molecular weight Emissions from Stationary Sources (Instrumental Analyzer Procedure) **USEPA 4** Determination of Moisture Content in Stack Gases (approximation Moisture content . method) Oxides of nitrogen USEPA 7E Determination of Nitrogen Oxides Emissions from Stationary . Sources (Instrumental Analyzer Procedure)  $(NO_x)$ Determination of Sulfur Dioxide Removal Efficiency and NO, emission rates USEPA 19 . Particulate Matter, Sulfur Dioxide, and Nitrogen Oxide Emission (lb/mmBtu) Rates Indicates a test parameter for each test run

Table 4-2Sampling and Analytical Methods

#### 4.1.1 Volumetric Flowrate (USEPA Methods 1 and 2)

USEPA Method 1, "Sample and Velocity Traverses for Stationary Sources" from the Code of Federal Regulations, Title 40, Part 60 (40 CFR 60), Appendix A, was used to select the sampling locations and determine the number of traverse points. The velocity measurement location and number of velocity traverse points are presented in the following table:

Table 4-3Sampling Location and Number of Traverse Points

Sampling	Duct	Duct	Duct	Number of	Traverse	Total	Cylconic
Locations	Diameter	Diameters	Diameters	Ports Used	Points per	Points	Flow
		Downstream	Upstream to		Port		Check
		to Flow	Flow				
		Disturbance	Disturbances				Average
	(inch)	(diameter)	(diameter)				Null Angle
Boiler 3	66	2.1	3.3	2	8	16	13

Figure 1 (see Figures Tab) depict the sampling location and traverse points.

Method 2, "Determination of Stack Gas Velocity and Volumetric Flow Rate (Type S Pitot Tube)," was used to measure flue gas velocity and calculate volumetric flowrate. An S-type Pitot tube and thermocouple assembly calibrated in accordance with Method 2, Section 10.0, connected to an electronic manometer was used during testing. Because the dimensions of the Pitot tube met the requirements outlined in Method 2, Section 10.1, and were within the specified limits, the baseline Pitot tube coefficient of 0.84 (dimensionless) was assigned. The electronic



manometer and thermometer have been calibrated using Calibration Standards which are traceable to National Institute of Standards (NIST). Refer to Appendix A for the Pitot tube, electronic manometer, and thermometer inspection and calibration sheets. Refer to Appendix B for sample calculations of flue gas velocity and volumetric flow rate.

**Cyclonic Flow Check.** Bureau Veritas evaluated whether cyclonic flow was present at the sampling location. Cyclonic flow is defined as a flow condition with an average null angle greater than 20°. The direction of flow can be determined by aligning the Pitot tube to obtain zero (null) velocity head reading—the direction would be parallel to the Pitot tube face openings or perpendicular to the null position. By measuring the angle of the Pitot tube face openings in relation to the stack walls when a null angle is obtained, the direction of flow is measured. If the absolute average of the flow direction angles is greater than 20 degrees, the flue gas is considered to be cyclonic at that sampling location and an alternative location should be found.

The average of the measured traverse point flue gas velocity null angles was:

• 13° from the direction of flow

The measurements indicate the absence of cyclonic flow at the Boiler No. 3 exhaust sampling location. Field data sheets are included in Appendix C. Computer-generated field data sheets are included in Appendix D.

#### 4.1.2 Molecular Weight (USEPA Method 3)

The carbon dioxide contribution to flue gas molecular weight was evaluated using Method 3, "Gas Analysis for the Determination of Dry Molecular Weight." Flue gas was extracted from the stack through a probe positioned near the centroid of the duct and directed into a Fyrite® gas analyzer. The concentrations of carbon dioxide (CO<sub>2</sub>) were measured by chemical absorption with a Fyrite® gas analyzer to within  $\pm 0.5\%$ . The average CO<sub>2</sub> result of the grab samples were used to calculate molecular weight.

#### 4.1.3 Moisture Content (USEPA Method 4)

The moisture content of the flue gas was measured using USEPA Method 4, "Determination of Moisture Content in Stack Gases." Bureau Veritas' modular USEPA Method 4 stack sampling system consists of:

- A stainless steel probe.
- Tygon<sup>®</sup> umbilical line connecting the probe to the impingers.
- A set of four Greenburg-Smith (GS) impingers with the configuration shown in Table 4-4 situated in a chilled ice bath.



- A length of sample line.
- An Environmental Supply<sup>®</sup> control case equipped with a pump, dry-gas meter, and calibrated orifice.

Impinger	Туре	Contents	Amount	
1	Modified	Water	~100 milliliters	
2	Greenburg Smith	Water	~100 milliliters	
3	Modified	Empty	0 milliliters	
4	Modified	Silica desiccant	~300 grams	

Table 4-4
<b>USEPA Method 4 Impinger Configuration</b>

Prior to initiating a test run, the sampling train was leak-checked by capping the probe tip and applying a vacuum of approximately 15 inches of mercury to the sampling train. The dry-gas meter was then monitored for approximately 1 minute to verify that the sample train leak rate is less than 0.02 cubic feet per minute (cfm). The sample probe was then inserted into the sampling port near the centroid of the stack in preparation of sampling. Flue gas was extracted at a constant rate from the stack, with moisture removed from the sample stream by the chilled impingers.

At the conclusion of the test run, a post-test leak check was conducted and the impinger train was carefully disassembled. The weight of liquid or silica gel in each impinger was measured with a scale capable of measuring  $\pm 0.5$  gram. The weight of water collected within the impingers and volume of flue gas sampled was used to calculate the percent moisture content. Refer to Figure 2 after the Figures Tab for a drawing of the USEPA Method 4 sampling train.

#### 4.1.4 $O_2$ and $NO_x$ (USEPA Methods 3A and 7E)

 $O_2$  and  $NO_x$  concentrations were measured following USEPA Methods 3A, "Determination of Oxygen and Carbon Dioxide Concentrations in Emissions from Stationary Sources (Instrument Analyzer Procedure)" and 7E, "Determination of Nitrogen Oxides Emissions from Stationary Sources (instrument analyzer procedure)." Sampling for  $O_2$  and  $NO_x$  consisted of extracting the flue gas from the stack through:

• A stainless-steel probe



- Heated Teflon sample line to prevent condensation
- A chilled Teflon impinger train with peristaltic pump to remove moisture from the sampled gas stream prior to entering the analyzer
- Thermo 42CHL NO<sub>x</sub> chemiluminescence and Teledyne paramagnetic oxygen gas analyzer gas analyzer

Data was recorded at 1-second intervals on a laptop computer equipped with data acquisition software (DAS). Recorded pollutant concentrations were averaged over the duration of each test run.

Prior to testing at the Boiler No. 3 stack, a 3-point stratification test was conducted at 17, 50, and 83% of the stack diameter for at least twice the response time. The results of the 3-point stratification demonstrated that sampling from a single point near the centroid of the duct was appropriate.

An NO/NO<sub>2</sub> conversion check was performed utilizing an approximate 50-ppmv NO<sub>2</sub> calibration gas. The NO concentration was greater than 90% of the introduced NO<sub>2</sub> calibration standard.

A calibration error check was performed by introducing zero-, mid-, and high-level calibration gases directly into the analyzers. The calibration error check was performed to evaluate the analyzers response within the acceptable  $\pm 2\%$  range of the calibration span.

Prior to each test run, a system-bias test was performed where known concentrations of calibration gases were introduced at the probe tip to measure if the analyzers response was within  $\pm 5\%$  of the calibration span. At the conclusion of each test run, an additional system-bias check was performed to evaluate the percent drift from pre- and post-test system-bias checks. If percent drift was less than 3.0% of span, the test is considered valid.

Figure 3 depicts the USEPA Method 3A and 7E sampling train. Calibration data along with the USEPA Protocol 1 certification sheets for the calibration gases used are included in Appendix A.

#### 4.1.5 NO<sub>x</sub> Emission Rate (USEPA Method 19)

USEPA Method 19, "Determination of Sulfur Dioxide Removal Efficiency and Particulate Matter, Sulfur Dioxide, and Nitrogen Oxide Emission Rates," was used to calculate the Boiler No. 3 NO<sub>x</sub> emission rates in units specified by the air permit. Oxygen concentrations and appropriate F factors (ratios of combustion gas volumes to heat inputs) were used to calculate NO<sub>x</sub> emission rates from measured NO<sub>x</sub> and O<sub>2</sub> concentrations. Specifically, Equation 19-1 from the method was used:



$$E = C_{d}F_{d} \frac{20.9}{(20.9 - \%O_{2d})}$$

Where:

Е		Pollutant emission rate (lb/million-Btu)
$C_d$	=	Pollutant concentration, dry basis (lb/scf)
Fd	=	Volumes of combustion components per unit of heat content (8,710 dscf/MM
		Btu for natural gas)
$O_{2d}$	=	Concentration of oxygen on a dry basis (%)

## 4.2 Recovery and Analytical Procedures

Recovery and analytical procedures were not applicable to this test program.

### 4.3 Cross-Sectional View Sketch

Figure 1 depicts the cross-sectional view and sampling port locations for the Boiler No. 3 source.



## 5.0 Test Results and Discussion

### 5.1 Results

The results of this testing program are summarized in Section 2.0 and presented in Table 1 after the Tables Tab. Graphs of the oxygen and oxides of nitrogen concentrations are presented in Graphs 1 through 3.

### 5.2 Significance of Results to Emission Regulations

The emissions results are used to evaluate compliance with emission limits for  $NO_x$ . Tables showing the results and air emissions limits in the applicable permit are presented in Section 2.0.

The results of this test program indicate Boiler No. 3 at the Nexteer Automotive facility is operating in compliance with permit limits.

## 5.3 Sampling Variations or Operating Conditions

No sampling variations or deviations were encountered during this test program. The boiler was operated greater than 90% capacity during testing.

## 5.4 Upset Conditions

No upset conditions were encountered during this test program.

## 5.5 Air Pollution Control Device Maintenance

No significant air pollution control device maintenance activities have occurred within the past three months.

## 5.6 Results of Audit Samples

Audit samples were not required during this testing program.



## 5.7 Calibration and Inspection Sheets

Calibration and inspection sheets are presented in Appendix A.

## 5.8 Sample Calculations

Sample calculations are presented in Appendix B.

### 5.9 Field Data Sheets

Field data sheets are presented in Appendix C. Computer-generated data sheets are presented in Appendix D. Facility operating parameters are presented in Appendix E.

## 5.10 Laboratory Data

Laboratory data was not required during this test program.



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## Table



# Table 1Boiler No. 3 O2 and NOx Emissions Results

## Nexteer Automotive

Saginaw, Michigan Bureau Veritas Project No. 11014-000059.00 Sampling Date: April 9, 2014

Parameter	Units	Run 1	Run 2	Run 3	Average
Start Time	hranin	10:45	12:00	13:10	
Duration	min	60	60	60	60
Steam Production	lb/hr	115,800	115,900	115,500	115,733
Fuel Consumption	MCF/hr	132	119	115	122
O <sub>2</sub> Trim Setting	%	50.5	50.5	50.5	50.5
Volumes of combustion component per unit of heat content (Fd)	dsef/mmBtu	8,710	8,710	8,710	8,710
Volumetric Flowrate (Q <sub>std, dry</sub> )	dscf/min	29,101	30,248	30,495	29,948
O <sub>2</sub> Concentration (Cave)	%	2.3	2.2	2.3	2.3
Pre-test system calibration, zero gas (Co)	%	-0.1	-0.1	-0.1	0
Post-test system calibration, zero gas (Co)	%	-0.1	-0.1	-0.1	-0.1
Certified low bracket gas concentration (CMA)	%	11.0	11.0	11.0	11.0
Pre-test system calibration, low bracket gas (C <sub>M</sub> )	%	10.3	10.3	10.3	10.3
Post-test system calibration, low bracket gas (CM)	%	10.3	10.3	10.3	10.3
Average Corrected O <sub>2</sub> Concentration (C <sub>g13</sub> )†	%	2.5	2,5	2.5	2.5
$NO_x$ Concentration ( $C_{avg}$ )	ppmvd	72.2	72.4	71.2	72.0
Pre-test system calibration, zero gas (Co)	ppmvd	0.6	0.8	1.0	0.8
Post-test system calibration, zero gas (Co)	ppmvd	0.8	1.0	3.3	1.7
Certified low bracket gas concentration (CMA)	ppmvd	45.7	45.7	45.7	45.7
Pre-test system calibration, low bracket gas (C <sub>M</sub> )	ppmvd	43.7	42.7	42.0	42.8
Post-test system calibration, low bracket gas $(C_M)$	ppmvd	42.7	42.0	44.6	43.1
Average Corrected NOx Concentration (Cgss)†	ppmvd	76.9	78.8	76.7	77.5
NO <sub>x</sub> Mass Emission Rate	lb/mmBtu	0.091	0.093	0.091	0.091
NO <sub>x</sub> Mass Emission Rate	lb/hr	16.0	17.1	16.8	16.6

t: corrected for analyzer drift

dscf/mmBtu: dry standard cubic feet per minuto/million British thermal unit

Co: average of the initial and final system calibration bias check responses from the low-level (or zero) calibration gas, ppmv

 $C_{\rm MA}$  : actual concentration of the upscale calibration gas,  $ppm\nu$ 

 $C_{M}$ : Average of initial and final system calibration bias check responses for the upscale calibration gas, ppmv

 $\mathbf{C}_{\mathbf{ga}}$  : Average effluent gas concentration adjusted for bias,  $\mathbf{ppmv}$ 

ppmvd: part per million by volume, dry basis

lb/scf: pound per standard cubic feet

lb/mmBtu: pound per million British thermal unit

lb/hour: pound per hour

O<sub>2</sub>: oxygen

NOx: oxides of nitrogen



# Figures

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